## Report for **Buildings Commissioner Robert D. LiMandri**

CTL, PC Project No. 500108

# **High Risk Construction Oversight Study**

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### **TABLE OF CONTENTS**



B.7 Site Safety B-40









## **Appendix II Principal Staff Resumes**

# **A. Executive Summary**

# **A.1 INTRODUCTION**

This report provides a compilation of findings and recommendations from the New York City Department of Buildings High Risk Construction Oversight (HRCO) study that was conducted from July 2008 through January 2009.

This chapter provides an overview of the study with a discussion of overall purpose and approach. At the end is a summary of the recommendations that resulted from the study.

Following chapters discuss results from the HRCO benchmarking study and general recommendations that apply broadly to New York City construction operations. The balance of the report is devoted to the specific studies and recommendations for highrise concrete, crane and excavation operations. The chapters on each of these operational areas reflect the specific characteristics of that area of study. Thus, while there is a general similarity among these chapters, there are also many differences in presentation that are necessitated by the differences in the approach and findings in each area.

## **A.2 DESCRIPTION OF THE HRCO STUDY**

In July 2008, The New York City Department of Buildings (DOB) initiated the High Risk Construction Oversight study (HRCO). This was precipitated by the March 15<sup>th</sup> and May 30<sup>th</sup> fatal crane collapses as well as a general increasing trend in occurrences of job-site accidents. DOB identified three high risk areas of study based on historical accident data: high-rise concrete, cranes and hoists, and excavation operations.

The goal of this study was to develop recommendations for modifications to the NYC regulatory framework and construction industry practices to improve safety. DOB retained CTL as the lead consultant on this effort. CTL partnered with organizations specializing specific to the high risk operations: Crane Tech Solutions (CTS), AECOM, Patuxent Engineering Group, Construction Safety Consultants and DBR Group.

The HRCO study was divided into five areas: high-rise concrete, cranes, excavations, personnel and material hoists, and the Department's regulatory framework. High-rise concrete comprised buildings greater than 15 stories, which reflects the 1968 building code definition. However, the recommendations are intended to apply to buildings greater than 10 stories, which is the high-rise definition in the 2008 building code.

The HRCO study included:

**Site Observations:** Systematic review of procedures on construction sites associated with high-risk operations.

**Review of DOB Operations:** Study of DOB's regulatory framework, permitting procedures, field inspections and staffing.

**Industry Outreach:** Site observation teams gathered feedback from construction crews at the selected construction sites on industry and DOB issues and conducted formal meetings with industry.

**Benchmarking**: Review of procedures and requirements of other jurisdictions.

The purpose of these activities was to identify patterns in the construction process associated with opportunities to improve safety.Thus, for example, site visits and permitting reviews were conducted to identify occurrences of safety issues common to multiple projects rather than exhaustively study safety aspects of any one specific construction project. A formal protocol was established at the onsite of the study by which HRCO field teams alerted DOB of potential safety issues for DOB response and enforcement as necessary.

Each operational team (high-rise concrete, cranes, excavations and hoists) included a principal and a field manager. The team principal was responsible for overall technical execution of the assessment of the operational area. The team field manager was

responsible for oversight of the day-to-day operations of the site observation teams, including assessment of DOB operations. The lead staff for the HRCO study are shown in Table A.1.





<sup>1</sup>Registered in a state other than New York

The participating firms of the study provided expertise in each of the high-risk areas. CTL staff investigated some of the most important construction accidents and failures of recent history, and are leaders in concrete building construction. For example, CTL senior advisor, W. Gene Corley, served as the Team Leader for the FEMA study of the World Trade Center attacks. The excavation team (STS/AECOM) provides excavation consulting services on some of the most challenging projects around the world, including record-setting high-rises such as the Chicago Spire. Crane Tech Solutions has decades of experience in crane design, inspection, maintenance and leasing services. Patuxent Engineering Group is one of only a handful of firms providing consulting expertise in temporary structures including construction hoists. DBR Group provided experience to critically assess the NYC regulatory framework. DBR Group

principal, Dennis Richardson, is a past building official and active member of building code committees.

In all, a staff of more than thirty experts participated in the study. Most principals are presidents and CEOs with decades of experience in their respective fields. The HRCO experts have practiced throughout the United States, both in New York City and outside. The teams' broad geographical range of experience provided a useful perspective to compare and contrast New York City construction practices with those prevailing in other dense urban areas that face similar public safety challenges.

## **A.3 STATISTICAL ASPECTS OF THE HRCO STUDY**

The HRCO study utilized statistical procedures to the greatest extent possible. Table A.2 provides a summary of historical DOB data related to construction operations. *Incidents* include any event at a job site that required DOB response and *accidents* are those incidents that caused injury, fatality or significant property damage. The high risk columns provide subtotals for high-rise concrete, cranes, excavations and hoists. As can be seen, the operations identified as high risk account for approximately 1/3 of accidents and ½ of fatalities. Additionally, the rate of injuries and fatalities per accident is typically higher for these four types of operations.



#### **Table A.2: HRCO review of DOB incident database (data from January 2, 2006 to January 13, 2009)**

Statistical aspects for each operational area are discussed in those chapters of this report. In general it must be recognized that the HRCO study, while substantial and methodical, was still limited to a relatively brief period of time (August – December, 2008) and a limited cross section of the NYC construction environment. Additionally, accidents associated with construction are generally indeterministic (random events that cannot be predicted with certainty) and are a function of human factors, materials, and equipment. In many instances the study relied on extrapolation and empirical assessment of observations. Results are based on the most well-considered assessment possible utilizing limited and variable data combined with the professional experience of the team and input from DOB and Industry.

The method used to preliminarily assess viability of the study is as outlined in ASTM E122 - Standard Practice for Calculating Sample to Estimate, With a Specified Tolerable Error, the Average for a Characteristic of a Lot or Process. This procedure provides a basis for determining meaningful sample sizes for indeterminate processes such as NYC construction operations. Table A.3 provides examples of sample size calculations.



#### **Table A.3: Sample Size Calculations per ASTM E122.**

The interpretation of Table A.3 is as follows:

- 1. **Population probability** is the rate of occurrence of a specific defect. For example, the percentage of construction sites that might exhibit a fall hazard.
- 2. **Error in estimating population probability**, relative to the example above this is the error in estimating the percentage of occurrences of fall hazards. In Table A.3 this is taken uniformly as 10% (thus the actual occurrence of fall hazards would be within 10% of the expected probability).
- 3. **Probability of exceeding error**, allows for the potential that the actual error will be greater than specified in item 2.
- 4. **Minimum sample size**, based on the acceptable error rates described above, this is the minimum sample size to properly observe the specified defect.

A rigorous application of this method to every facet of the high risk operations is not practical. However, relative to the "defect rates" that were observed in NYC, ASTM E122 indicates that the number of site observations conducted during the HRCO study were of reasonable order to characterize the operations. Summaries of site observation totals and geographical distribution are provided in Table A.4 and Figure A.1.



#### **Table A.4: Summary of HRCO Site Observation Totals.**

For example, the fall hazard risk of not tying-off was observed at 31% of high-rise concrete sites. Going back to table A.3 shows that approximately 81 site observations would be necessary to properly observe a defect that occurs at this rate, and with the specified error limits. Thus the HRCO total of 181 site safety site visits at 94 unique sites (see High-rise Concrete chapter) should be sufficient to characterize tie-off violation issues.



**Figure A.1: Distribution of site observations.** 

## **A.4 INDUSTRY OUTREACH**

The general approach of engaging industry was similar and two-phased among the operational teams (high-rise concrete, cranes, excavations and hoists). One primary method of industry outreach was accomplished at job sites, by gathering feedback from construction staff. The other method was through formal subcommittee meetings with a cross-section of industry stakeholders.

In addition to these two methods each operational team conducted other forms of outreach as guided by particular aspects of the study (e.g. the high-rise concrete team observed operations at a union training facility). Major industry meetings conducted as part of the study are presented in Table A.5.



### **Table A.5: HRCO Industry Outreach Meetings.**

Industry subcommittees were formed by soliciting participation from professionals, and, in the case of cranes, major manufacturers. Each operations group conducted at least two monthly meetings. The first meeting was primarily devoted to presentation of

developing recommendations. Follow up meetings were focused on refining the final recommendations. Relevant source data (as available) and draft summaries were provided in advance of the meetings to industry and DOB. Subcommittee participants were invited to comment on interpretation of the presented data; individual experiences; scope and content of the proposed recommendations; feasibility of implementation; and, perceived effectiveness and anticipated compliance with the potential recommendations. Participants were also encouraged to suggest alternative or supplemental recommendations based on knowledge of local practice and experience with the existing regulatory process. Participating stakeholders are shown in Table A.6.



#### **Table A.6: HRCO Industry Stakeholders.**

## **A.5 SUMMARY OF RECOMMENDATIONS**

The culmination of the HRCO study was development of more than sixty recommendations to improve safety during high-risk construction operations. Separate chapters for each operation detail the development and content of these recommendations. Below is a table summarizing all of the recommendations. The table includes each recommendation name and ID, a paraphrase of the recommendation language, a key observation associated with the recommendation and identification of *further study* items. The recommendation ID uses HC (high-rise concrete, C (crane), E (excavation) and H (hoist). *Further Study* recommendations, as the designation implies, are those for which there is clear indication safety improvements are possible, but specific and necessary details of the recommendation require additional study. The *key observation* provides a single example of the supporting data to provide a degree of context for the recommendation.

Recommendations that are not identified as Further Study may still require analysis or alteration as they are being implemented. And all recommendations, whether or not Further Study, should be subjected to on-going review after implementation to assess whether the desired affect is being achieved.

It is important to appreciate that this study was motivated by construction accidents and had the sole purpose of generating recommendations for changes to construction operations and regulatory practices to improve safety. Thus, by its very nature, the focus of the study was to identify areas in which there is opportunity for significant improvement.

New York City is a dynamic and challenging environment in which to undertake construction. Many of the leading design and construction companies in the world have sole or primary practices in New York City. Thus, the HRCO team did not lightly take on the task of providing these recommendations. In a number of instances the recommendations were generated by observing positive practices that are already in place by many in the industry and recognizing that the practice should be adapted universally.

Lastly, the HRCO team recognizes that a number of recommendations apply beyond the subject operational area. This is particularly relevant, for example, regarding site safety and fall hazard recommendations. These were motivated by high-rise concrete accidents, but similar risks occur with steel and masonry construction. The degree and manner in which recommendations should be applied to other construction operations should be carefully considered as the recommendations are implemented.

### **High-Rise Concrete - Formwork**



### **High-Rise Concrete – General Site Safety**



### **High-Rise Concrete – Worker Falls**



## **High-Rise Concrete – Special Inspections and Construction Quality**



### **High-Rise Concrete – Plan Review**



## **Excavations**



# **Crane – Equipment Design**



## **Crane – Site Specific Design**



### **Crane – Crane Operations**



### **Crane – Inspections**



Key Observation: Less than 10% of hoists had been properly inspected during required "drop test".

### **Crane – Maintenance and Repair**



## **Cranes – Department of Buildings' Operations**



# **B. High-rise Concrete**

# **B.1 INTRODUCTION**

This chapter summarizes the high-rise concrete construction assessment, and includes this introduction (Section 1), methodologies used to conduct the assessment (Section 2), studies and observations completed in addition to the assessments (Sections 3 and 4), and a summary of the recommendations (Section 5). CTL principally authored this chapter.

The High Risk Construction Oversight (HRCO) Team encountered great interest and desire on the part of the construction industry to increase safety on active construction sites. At the same time, during the observation of day-to-day construction operations throughout New York City, it became clear that there is substantial need for changes in the current construction practices and behaviors to actually achieve an increase in site safety. As with the NYC construction industry's past efforts to establish an awareness that hard-hats must be worn on construction sites, a program that required a committed long-term campaign, there are many facets of the construction process which will require a targeted, disciplined approach to actually achieve the universally agreed goal of improved safety. This is true of nothing so much as the need to greatly improve the current practice regarding fall protection. In this case there are sufficient regulations in place, but compliance is poor. Penetrating and changing this aspect of construction culture will require resolve by DOB and industry.

A primary theme that became apparent during this assessment is the need for modernization in the construction processes utilized in New York City by contractors. For example, modernization of current formwork practices could improve at least three safety issues: personnel fall hazards; material fall hazards; and, the structural integrity and safety of the formwork. Personnel fall hazards are associated with the labor-intensive nature of formwork construction and stripping, much of it needing to occur near the building edges, and the efforts required to provide effective fall restraints near these edges. Material fall hazards are related to the significant amount of loose material that is kept on the construction floors. Structural integrity is associated with the importance of designing and constructing the formwork to support substantial loads from wet concrete and the challenge of providing proper inspection.

Each of these three safety issues is made more challenging by the wide-spread use of stickbuilt forms in New York City. By comparison, the overwhelming majority of municipalities surveyed by the HRCO use prefabricated concrete forming systems for major projects<sup>1</sup>. Prefabricated forms offer advantages of built-in anchorage systems, more efficient control of onsite materials, and more uniform structural integrity. This is not to say that stick-built formwork can not be used safely, but it must be recognized that this outmoded forming system serves more to impede than promote safety.

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<sup>&</sup>lt;sup>1</sup> See Formwork Recommendations

In similar ways modernization applies to the procedures utilized during construction inspection, concrete reinforcing steel fabrication and placement, documentation of field changes and monitoring of site safety.

## **B.2 SITE OBSERVATION**

A total of 279 site observations were completed by HRCO field teams between August and November 2008. The two-person observation teams typically consisted of an Engineer and Safety Expert. *Targeted* site visits were limited to safety issues only. *Full* site visits included safety and engineering observations. A member of the DOB Building Enforcement Safety Team (BEST) accompanied the HRCO observation teams during a substantial number of site visits.

Sites were selected, and visited randomly, from a list of addresses with permit applications for concrete-framed buildings filed after January 1, 2008, and therefore likely to be actively engaged in construction activity (i.e.; an active site). The entire population of "Major"<sup>2</sup> buildings was selected from this list. In addition to these Major buildings, the HRCO observation teams visited the site of a limited number of other buildings<sup>3</sup>. Site observation data is summarized below. Detailed site observation summaries are provided in Appendix B.1.



**Table 1: Active Site Visits<sup>4</sup>**

 $2$  At the time of observation, the 1968 NYC Building Code definition was used (structures exceeding 15 stories, heights of 200', or footprint areas of 100,000 SF).

 $3$  Buildings with fewer than 15 stories

<sup>&</sup>lt;sup>4</sup> Includes multiple random repeat visits at particular addresses



### **Table 2: Distinct Site Observations at Active Sites**

Observation procedures included the following.

- A survey of the building site was conducted using a standardized *Location Report* form. Additional information, gleaned from interviews or observations not directly addressed by the Location Report format, was entered as comments.
- Interviews were conducted with construction staff and site safety personnel
- Photographic documentation of representative safety and quality conditions
- Relaying critical safety and/or construction conditions to the Department of Buildings

## **B.3 SUMMARY OF ADDITIONAL ASSESSMENTS AND OBSERVATIONS**

Additional observations and assessments were made outside the scope of standard site observation procedures. These additional tasks gauged the accuracy of five selected concrete testing laboratories, assessed the quality of concrete laboratory testing and reporting at three facilities, and assessed the level of rebar fabrication and placement training offered by the Metallic Lathers and Reinforcing Ironworkers Union Local 46, during a visit to their Queens, New York training facility.

## **B.3.1 Comparative Concrete Testing**

Concerns were raised regarding the concrete sampling and testing methods typically employed throughout the City. Specifically, the ability of testing labs to adequately perform both code compliant sampling methods, and produce accurate test results were assessed by the HRCO team during the fall of 2008.

Ten active concrete sites were randomly selected for additional observation. These selected sites ultimately encompassed five separate independent testing agencies. HRCO staff prepared cylinders and observed as personnel from the testing agencies made additional concrete test cylinders in the field, which HRCO staff delivered to an independent laboratory (the laboratories of The Port Authority of New York and New Jersey) for testing (see Appendix B.2).

Concrete strength test results from the laboratories of The Port Authority of New York and New Jersey were compared with the test results produced by the independent testing agencies. In general, the HRCO team found that the strength test results from the independent testing agencies compared favorably with the results from The Port Authority Laboratories.

## **B.3.2 Laboratory Quality Observations**

The HRCO observed test procedures at selected testing facilities (Appendix B.3). These observations revealed significant variability in laboratory quality which warrants the Department's continued monitoring of the laboratory's ability to perform ASTM-compliant testing.

The Department has taken steps recently to raise the standards for concrete testing laboratories by requiring laboratories to be accredited under the American Association of Highway and Transportation Officials (AASHTO) Accreditation Program (AAP), the National Voluntary Laboratory Accreditation Program, or an equivalent accrediting agency. Previously approved concrete testing laboratories must achieve amended accreditation by July 1, 2010. In addition, the Department has also increased the knowledge base of inspectors regarding field testing requirements through enrollment in nationally recognized field testing certification programs.

## **B.3.3 Union Training Facility**

HRCO Engineers visited the Training Facility of the Metallic Lathers and Reinforcing Ironworkers Union, Local 46 in Woodside, Queens on January 21, 2008. Discussions with union

representatives highlighted both the practical and classroom training methods employed to promote proper rebar fabrication and placement best practices. HRCO staff observed the following:

- Extensive classroom facilities and availability of educational materials
- Practical, hands-on learning environments, including full-scale slab, beam and posttensioning mockups.
- Practical hands-on fabrication instruction, including typical field-bending equipment.

According to the union representatives, field fabrication methods can provide quality and consistency levels commensurate with shop-bent reinforcing if proper bending techniques are utilized.

## **B.4 DOB PROCESS REVIEW**

In conjunction with our observations of activities on a number of construction sites, the HRCO team had the opportunity to work with and observe Department of Buildings operations related to construction site safety. The HRCO worked directly with the Building Enforcement Safety Team (BEST), and reviewed their procedures for selecting sites for inspection and methods of conducting inspections.

The HRCO also reviewed DOB operations related to conducting technical reviews of plans and documenting incident and accident investigations.

These departmental assessments are reflected in the recommendations.

### **B.5 SUMMARY OF RECOMMENDATIONS**

Recommendations fall into subcategories based on working areas of operation, including formwork design and construction, general site safety practices and procedures, special inspection practices and construction quality, worker fall hazards, and plan review. Within these five operational areas, recommendations may be classified as either direct, or those requiring further study. Further study recommendations may require additional investigation on the part of the DOB to fully gauge their applicability. Recommendations are summarized as follows.

### **B.5.1 Formwork**

### **Formwork Design Requirements (HC-1)**

Require essential specification information to be included on stamped formwork designs. Essential specifications shall include information required in chapter 6 of ACI 318. At a minimum, critical information such as reshoring sequences and schedules, required numbers of reshored floor levels, lumber material grade and rated stress, structural configuration and spacing of structural members, vertical formwork design, nailing schedules, and lateral bracing sequences and requirements shall be included.

### **Protection of Existing Construction (HC-2)**

Require thresholds for the production of stamped and sealed formwork designs to include instances where adjoining structures are used directly or indirectly to support formwork.

### **Formwork Special Inspection (HC-3)**

Require regular special inspection of formwork and reshore installations preferably by the formwork engineer of record, for structural integrity, conformance to essential specifications and the design intent.

### **Formwork Lateral and Wind Load Design (HC-4)**

Clarify wind design requirements pertaining to formwork to incorporate oblique wind loads. Wind resistant design of formwork should conform with national standards for temporary construction, such as the American Society of Civil Engineers, Design Loads on Structures During Construction (ASCE 37).

### **Formwork Construction for Wind Resistance (HC-5)**

Require perimeter formwork decking to be positively secured against uplift.

### **Wind Monitoring (Further Study, HC-6)**

Require continual measurement of wind speed and direction during construction at prescribed elevations. Provide an audible early warning system to alert workers to possible wind danger.

### **Wind Tunnel Studies (Further Study, HC-7)**

Conduct wind tunnel studies to observe and characterize wind behavior, and the resulting loads, along the perimeter of a completed concrete forming system. Further, conduct wind tunnel studies to observe and characterize wind behavior, and the resulting loads, throughout the field of a completed concrete forming system.

### **B.5.2 General Site Safety**

### **DOB Inspector Qualifications (HC-8)**

Enhance level of knowledge among DOB inspectors to include qualifications consistent with current NYC Building Code requirements regarding site safety practices, proper concrete formwork installation, and proper shoring and reshoring placement.

#### **DOB Inspection Procedures (HC-9)**

Update and publish standard sets of inspection protocols to create a consistent and uniform level of enforcement.

### **Housekeeping Requirements (HC-10)**

Clarify specific housekeeping requirements in inspection protocols.

### **Site Safety Hierarchy (Further Study, HC-11)**

Require site safety personnel's line of accountability to lead to owner (and not to the contractor or CM) to avoid a conflict of interest.

### **Upgrading Netting Requirements (Further Study, HC-12)**

Study effectiveness of enhancing existing netting requirements

#### **Material Handling (Further Study, HC-13)**

Establish requirements for the use of outrigger systems for material handling.
## **B.5.3 Worker Falls**

#### **Fall Hazard Awareness (HC-14)**

Implementation of a fall hazard awareness campaign through the use of posters, ads, and training at each jobsite for workers before they are allowed on site

#### **Contractor Documentation (Further Study, HC-15)**

Require contractor to document remedial actions taken when workers are identified as non-compliant regarding safety measures, including tie-off requirements. Remedial actions could include additional training sessions, suspension, or removal from job site.

#### **Repeat Offense Enforcement (Further Study, HC-16)**

Require a "two strikes and you're out" provision to be levied against the contractor in the event the contractor fails to enforce safety regulations and procedures. This clause would require that the project is shut down a prescribed number of days after a predetermined number of code violations or reportable incidents. The purpose of the shut down is to provide the contractor a period of time to properly implement safety measures.

## **B.5.4 Special Inspections and Construction Quality**

#### **Special Inspection Rule (HC-17)**

Strengthen outreach to industry on Special Inspection qualifications, and enforce the requirement that all Special Inspectors are properly registered and/or certified in compliance with NYC Special Inspection Rule requirements, effective July 1, 2009.

#### **Field Inspection (HC-18)**

Enhance level of knowledge among DOB inspectors to include qualifications consistent with the current NYC Building Code, specific to ACI Special Inspector training, to promote consistent enforcement of concrete practices, including field testing procedures.

#### **Inspection of Testing Labs (HC-19)**

Enhance level of knowledge among DOB personnel to include qualifications consistent with the current NYC Building Code, specific to ACI Special Inspector training, to promote consistent inspection of laboratory practices and conditions.

#### **Reinforcing Bend Quality Assurance (HC-20)**

Require documentation through photo and/or video that site bending practice complies with accepted industry standards and tolerances. Conformance may be spot checked by the DOB through inspection of logs and field conditions*.* 

#### **Reinforcing Placement Quality Assurance (HC-21)**

Require documentation through photo and/or video that steel placement complies with accepted industry standards and tolerances. Conformance may be periodically spot checked by the DOB through inspection of construction logs and field conditions*.* 

#### **B.5.5 Plan Review**

#### **Monitoring of Peer Review (HC-22)**

Retain professional engineers on behalf of DOB to monitor that peer reviews of identified projects are properly conducted as required by the NYC Building Code.

#### **Structural Drawing Information (HC-23)**

Require minimum level of information to be included on structural building drawings, including member end reactions and details with sufficient information to properly convey the design intent.

#### **Monitoring of Structural Information Quality (HC-24)**

DOB should retain professional structural engineers to review drawings to verify that the minimum level of structural information is contained on each set of structural drawings, shop drawings, and formwork drawings. Information to include requirements contained in ACI publications as noted in current NYC Building Code.

#### **Monitoring Constructability (HC-25)**

DOB should retain professional structural engineers to audit and verify that a sufficient, minimum level of details and detailing is included on each set of structural drawings and shop drawings. Minimum level of detailing to comply with requirements of ACI publications as noted in current NYC Building Code.

## **B.6 FORMWORK ISSUES**

### **B.6.1 Description**

The High Risk Construction Oversight (HRCO) High-Rise Concrete Team has observed numerous occurrences of inadequate design, construction, and inspection of formwork assemblies. In addition, due to the observed susceptibility of site-constructed dimension lumber (stick) formwork assemblies (Figure B.6.1) to wind and other lateral loads, the High-Rise Concrete Team concluded the current wind lateral load design criteria is not adequate. Based on HRCO team observations, formwork design in New York City typically considers only gravity loads and seldom, if ever, considers lateral loads due to wind loads or lateral loads due to accidental eccentricity of the gravity support system.

The High-rise Concrete Team, utilizing engineers under the supervision of a New York State Registered Professional Engineer, inspected 98 active HRCO sites. These sites included both union and non-union projects. Of the 98 site investigations, critical formwork deficiencies where construction or design deficiencies created imminently hazardous conditions, were found at fifty-seven percent (57%) of the sites. Observed formwork defects (Tables 1-2, Figures B.6.2-B.6.5) included both design and construction deficiencies. Deficient conditions include the following.

- Insufficient level of design information on the formwork drawings
- Construction not in conformance with the design intent
- Ineffective and insufficient inspection



**Figure B.6.1: Typical Stick Formwork Assembly consisting of Timber Posts and Lumber Framing Elements** 

	<b>All Active</b> <b>Sites</b>
<b>Number of Fully Inspected Sites</b>	98
<b>Number of Observed Formwork</b> <b>Construction and Design Defects</b> <b>Deemed Critical</b>	56 (57%)

**Table 1: Observed Formwork Defect Rates** 

#### **Table 2: Typical Critical Formwork Defects**

No Stamped Formwork design (as required by NYC Building Code)

Formwork construction not in conformance with design

Premature stripping or premature reshore removal (as required by design)

Insufficient number of reshored floors (as required by design)

Insufficient number of shored floors (as required by design)

Insufficient number or improperly installed lateral braces (as required by design)

Insufficient post spacing (as required by design)

Insufficient design data regarding sequencing of form removal or adequate concrete strength

Premature removal of lateral bracing (as required by design)

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**Figure B.6.2: Formwork Construction Not in Conformance with Design, Unstable Timber Posts used as Filler between Steel Shoring Tower and Concrete Soffit** 



**Figure B.6.3: Improved Filler Material Installation (Laid Horizontally) between Steel Shoring Tower and Concrete Soffit** 



**Figure B.6.4: Formwork Construction not in Conformance with Design, Damaged Timber Post** 



**Figure B.6.5: Insufficient Post Spacing, Missing Posts at Stringer Element (Top Center)**

## **B.6.2 Recommendation HC-1: Design Requirements**

*Require essential specification information to be included on stamped formwork designs. Essential specifications shall include information required in chapter 6 of ACI 318. At a minimum, critical information such as reshoring sequences and schedules, required numbers of reshored floor levels, lumber material grade and rated stress, structural configuration and spacing of structural members, vertical formwork design, nailing schedules, and lateral bracing sequences and requirements shall be included.* 

Critical design defects (Table 3), such as the failure to properly prescribe the number of reshored floor levels required to support formwork assemblies, place critical engineering decisions that affect the performance of the structure in the hands of unqualified persons at the site. Contractors often lack the requisite experience and knowledge necessary to judge the adequacy of an engineering design, and can only assume a properly stamped & sealed formwork design drawing contains sufficient design information.

Number of Fully Inspected Site Observations	98
<b>Number of Critical Formwork Defects</b>	56 (57%)
Number of Critical Formwork Defects Attributable to Design	25 of 56 (45%)

**Table 3: Critical Formwork Defect Origin** 

## **B.6.3 Recommendation HC-2: Protection of Existing Construction**

*Require thresholds for the production of stamped and sealed formwork designs to include instances where adjoining structures are used directly or indirectly to support formwork.* 

Currently, formwork assemblies in excess of fourteen feet, constructed of two-stage shores, supporting power buggies, or supporting loads in excess of 150 psf require stamped and sealed formwork design drawings<sup>5</sup>. Recent incidents however, have highlighted a failure of the industry to properly address the effect of concrete pressures on adjacent structures (Figure B.6.6). While the HRCO recognizes the Engineer of Record is ultimately responsible for the stability and integrity of any adjacent walls exposed during construction or demolition, clear requirements addressing concrete placement are needed.

Current building code requirements read in part: *When any construction or demolition operation exposes or breaches an adjoining wall...the person causing the construction shall, at his own expense perform the following:* 

 *1. Maintain the structural integrity of such walls, have a registered design professional investigate the stability and condition of the wall, and take all necessary steps to protect such wall.*<sup>6</sup>

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<sup>&</sup>lt;sup>5</sup> See BC 1906.3 Design of Concrete Formwork

<sup>&</sup>lt;sup>6</sup> See BC 3309.8 Adjoining Walls



**Figure B.6.6: Wall Failure Attributed to Concrete Pressures Imparted by Adjacent Construction**

## **B.6.4 Recommendation HC-3: Formwork Inspection**

*Require regular special inspection of formwork and reshore installations preferably by the formwork engineer of record, for structural integrity, conformance to essential specifications and the design intent.* 

Currently, formwork assemblies are self-inspected by the contractor installing the formwork; clearly presenting a critical conflict of interest. Construction defects (Table 4) account for more than seventy-five percent (75%) of observed formwork deficiencies (Figures B.6.8-B.6.11), and improper construction practices such as premature removal of formwork, or failure to install large portions of specified lateral bracing elements, present a critical hazard to worker and public safety.



#### **Table 4: Critical Formwork Defect Origin**



**Figure B.6.7: Construction Loads can be Significant<sup>7</sup> . Verification of Proper Formwork Assembly is Critical** 

 $7$  Configuration Shown Likely to Exceed 150 Pounds per Square Foot



**Figure B.6.8: Unstable<sup>8</sup> Stacked Truss-Type Stringer Assembly, Not in Conformance with Design** 

<sup>&</sup>lt;sup>8</sup> Prone to failure through twisting (Lateral Torsional Buckling) of wood truss elements



**Figure B.6.9: Stacked Engineered Lumber Formwork Failure in Queens Attributed to a Lack of Lateral Bracing.** 



**Figure B.6.10: Lack of Adequate Support under Post Base (Center), Not in Conformance with Design.** 



#### **Figure B.6.11: Improper Lateral Bracing Installation, Not in Conformance with Design. Lateral Braces are not Secured to Slab, Unable to Resist Load Reversals**

Existing contractor-managed inspection procedures have failed to ensure proper conformance to design specifications. These inspections require oversight by a qualified individual. Inspection requirements should include the following:

- Inspection of initial formwork installation for general conformance with the design to establish contractor familiarity with proper installation practices and procedures.
- Inspection of subsequent similar formwork installations for general conformance on a regular basis
- Inspection of critical formwork elements such as multi-tier tower assemblies and outriggers for general conformance commensurate with floor cycle times.
- Inspection of formwork installations with irregular configurations for general conformance to establish contractor familiarity with proper installation practices and procedures.
- Inspection of subsequent similar irregular formwork installations for general conformance on a regular basis

As an example, as recently as March  $12<sup>th</sup>$ , 2009, a vertical formwork failure occurred at 450 W. 14<sup>th</sup> Street, presenting a significant falling concrete and debris hazard to those below. Initial reports indicate the contractor-inspected vertical formwork configurations were not in conformance with the formwork design. Appropriate numbers of form ties were not installed (Figure B.6.12), leading to a blow-out failure and concrete spillage (Figure B.6.14). Supplemental inspection by a special formwork inspector or the formwork designer would have likely identified this insufficiently-constructed installation.

Subsequent protective action by the Department of Buildings included a mandatory reinspection by the formwork designer prior to resuming work, and required production of signed and sealed written procedures for future placements.



**Figure B.6.12: Vertical Formwork Configuration, Missing Walers Specified by Formwork Designer** 



**Figure B.6.13: Typical Proper Waler Installation (Wall, Left)** 



**Figure B.6.14: Spilled Concrete after Form Blow-out Restrained by Horizontal Netting (Center)** 

Table 5 provides a comparison of formwork design, construction and inspection requirements from both the 1968 and 2008 NYC Building Codes. Figure B.6.15 provides direct citations for inspection requirements.

The provisions in the two codes are very similar with the exception of the inspection requirements. The 1968 Code requires inspection for geometric accuracy of the formwork by an architect or engineer. It also requires a check to verify that the in place formwork conforms to the drawings. Furthermore, the 1968 code requires periodic inspections to detect incipient problems. This check may be done by the person supervising the work.

The 2008 Code requires that a *qualified person* inspect for geometric accuracy.

The 1968 provision of checking conformance to the drawings and periodic inspections for "incipient problems" is an important aspect of assuring the structural integrity of the formwork (though it would be better if the Registered Design Professional for the formwork were also required to conduct this inspection rather than the superintendent).



#### **Table 5: Comparison of Formwork Provisions in the NYC 1968 and 2008 Building Code.**

#### **2008 NEW YORK CITY BUILDING CODE**

**1906.2 Inspection.** Formwork, including shores, reshores, braces and other supports, shall be inspected prior to placement of reinforcing steel to verify that the sizes of the concrete members that are being formed conform to the construction documents and form design drawings. Such inspections shall be performed by a qualified person designated by the contractor. Subsequently, inspections shall be performed by such person periodically during the placement of concrete. During and after concreting, the elevations, camber, and vertical alignment of formwork systems shall be inspected using tell-tale devices. A record of all such inspections shall be kept at the site available to the commissioner. The names of the persons responsible for such inspections and the foreman in charge of the formwork shall be posted in the field office.

#### 1968 NYC Building Code

(1) Formwork, including shores, reshores, braces, and other supports, shall be inspected by an engineer or architect to verify the sizes of the concrete members being formed, as provided in article five of subchapter ten of this chapter. In addition, such forms shall be inspected for conformance with the form design drawings, when such drawings are required by the provisions of subdivision (c) of this section; and/or conformance with the provisions of this section. Such inspections may be made by the person superintending the work. Both such inspections shall be made prior to placement of reinforcing steel. Subsequently, inspections shall be made by the person superintending the work periodically during the placement of concrete to detect incipient problems.

(2) During and after concreting, the elevations, camber, and vertical alignment of formwork systems shall be checked using tell-tale devices.

(3) A record of all such inspections shall be kept at the site available to the commissioner, and the names of the persons doing the inspecting and the name of the foreman in charge of formwork shall be posted in the field office.

#### **Figure B.6.15: Code Requirements**

#### **B.6.5 Recommendation HC-4: Lateral and Wind Load Design**

*Clarify wind design requirements pertaining to formwork to incorporate oblique wind loads. Wind resistant design of formwork should conform with national standards for temporary construction, such as the American Society of Civil Engineers, Design Loads on Structures During Construction (ASCE 37).* 

As observed by High-rise concrete inspection teams, formwork is typically not securely anchored in place and has no inherent ability to resist the effects of wind loads. As a result, during the period of time between formwork erection and concrete placement, formwork that is subject to wind loads is susceptible to collapse or displacement. Although the occurrence of significant wind storms is rare and there is limited historical documentation of wind-related formwork failures (Table 6), when wind related formwork failures have occurred, these events have caused life threatening damage (Figures B.6.16-B.6.17).

Modified design criteria may also include considerations for exposure conditions as, historically, wind events are prevalent at western water exposures (Figure B.6.18).

The ASCE 37 standard prescribes applicable loads to be considered during the design of temporary structures such as formwork. The standard considers the temporary nature and short load duration when establishing the magnitude of load to be used in design. Lateral loads included in ASCE 37 that apply to formwork design are horizontal construction loads and wind loads. Relative to wind load criteria on temporary structures, ASCE 37 references ASCE 7, *Minimum Design Loads for Buildings and Other Structures* as the basis.



**Figure B.6.16: Formwork Failure at Hudson River Exposure** 



**Figure B.6.17: Formwork Failure in Reported 30-40 mph Winds** 







**Figure B.6.18: Historic Formwork Failures due to Wind Events** 

Loading criteria for formwork has been reviewed by cross-reference of applicable enforceable codes. The following compares the criteria and differences between the various codes.

Codes reviewed for this study were OSHA 1926.703, OSHA Subpart L, ANSI A10.9-2004, NYC 1968 Building Code and 2008 Building Code, ASCE 7-02 *Minimum Design Loads for Buildings and Other Structures*, ASCE 37-02 *Design Loads on Structures During Construction*, and ACI 347-04 *Guide to Formwork for Concrete*.

The ANSI A10.9-2004 was found to be the most commonly referenced standard. Both the 1968 and 2008 NYC codes reference this ANSI standard. Also, both codes contain design criteria similar to design criteria contained in this ANSI standard.

Lateral loading found in ANSI 10.9, Section 7.2.1, is defined as the following.

The greater of 100 plf along the form edge

• 2% of the total dead load on the floor distributed along the slab edge

Wind requirements of ASCE 7 include a minimum criteria of 15 psf and reduced wind speeds reflecting reduced probability of storm events for temporary construction. By comparison the NYC Building Code has similar criteria regarding 100 plf at the form edge and 2% of the dead load. The lateral wind load and uplift is addressed as a specific wind pressure within the NYC code RS9-5.

Uplift is addressed within ASCE 7-02, and is included in Chapter 6 as the upward load on the underside of overhangs and canopies. ASCE 7-02 also provides basic wind speed data for coastal areas, prone to hurricane activity, such as New York City.

ASCE 37-02 *Design Loads on Structures during Construction* lists factors that reduce the basic wind speed found in ASCE 7-02 according to an assumed construction period that is less than 5-years. According to ASCE 37, the construction period shall be taken as the time interval from first erection to structural completion of each independent structural system.

Based on an estimated construction period, a factor is given in ASCE 37. That factor reduces the basic wind speed found in ASCE 7 such that the reduced design wind velocity would have the same probability of being exceeded during the construction period as the 50-year mean recurrence interval design wind has during a 50-year period.

#### **B.6.6 Recommendation HC-5: Formwork Construction for Wind Resistance**

#### *Require perimeter formwork decking to be positively secured against uplift.*

Historically, DOB incident data indicates formwork failures have involved leading edge elements, such as unsecured plywood sheeting that was lifted by the wind along building perimeters. Although some formwork designers provide nailing schedules for decking elements, many designs improperly rely on the self-weight of the assembly alone to resist overturning and liftoff. Requirements for positive connection between decking and rib elements are needed to increase structural integrity of perimeter elements. Although modular engineered formwork systems (Figure B.6.19) require nailed connections between decking and rib elements in the same manner as "stick" assemblies, such systems also provide the added benefit of automatic, positive connection between towers, stringers, and ribs. Usage of such modular systems is commonplace (Table 7).



## **Table 7: Formwork Type Usage**



**Figure B.6.19: Modular Engineered Formwork System** 

### **B.6.7 Recommendation HC-6: Wind Monitoring (Further Study)**

*Require continual measurement of wind speed and direction during construction at prescribed elevations. Provide an audible early warning system to alert workers to possible wind danger.* 

Wind velocity and direction are highly sensitive to site-specific characteristics such as terrain, exposure, and surrounding structures. Thus, measurements of wind speed at remote locations $^{\rm 9}$  are not reliable surrogates for all localities when construction safety is in question. Site-specific wind readings will provide Site Safety Managers with the data necessary to mitigate wind-induced hazards. In addition, the Department of Buildings may use this additional site-specific wind data to refine wind-related code requirements.

Wind monitoring technology is established, and has been utilized most notably at 200 Murray Street, a high-rise construction site<sup>10</sup> which incorporated ultrasonic anemometers and remote data loggers.

#### **B.6.8 Recommendation HC-7: Wind Tunnel Studies (Further Study)**

*Conduct wind tunnel studies to observe and characterize wind behavior, and the resulting loads, along the perimeter of a completed concrete forming system. Further, conduct wind tunnel studies to observe and characterize wind behavior, and the resulting loads, throughout the field of a completed concrete forming system.* 

A review of current literature indicates little guidance exists regarding the behavior and resulting loads that are caused by wind on the leading edges of a concrete forming system at the perimeter of a building. Likewise, little was found as a guide regarding wind loads throughout the field of a completed concrete forming system.

<sup>&</sup>lt;sup>9</sup> NYC wind speeds are commonly measured at LaGuardia Airport, Newark Airport, and Central Park

<sup>&</sup>lt;sup>10</sup> The Goldman Sachs Building, supervised by Tishman

# **B.6.9 Additional HRCO Data**





<sup>11</sup> Borough of Brooklyn

<sup>12</sup> Borough of Manhattan







# **B.7 SITE SAFETY**

## **B.7.1 Description**

The High Risk Construction Oversight (HRCO) High-Rise Concrete Team documented numerous instances of unsafe jobsite conditions and developed recommendations to mitigate these hazards. Unprotected edges (fall hazards) were observed to have the greatest potential to endanger the safety of the public as well as that of construction workers themselves (Figures B.7.1-B.7.3). Other aspects of construction such as noncode compliant storage of material throughout the construction site, especially on stripping floors, provide unsafe conditions relative to egress and sources of wind-blown debris. The hazard of falling debris is ever present in New York City. Between January 2006 and June 2008, DOB records list over 200 falling material incidents, most from floors with active stripping operations. Seven significant debris incidents presenting a hazard to the public occurred during the month of March 2009 alone, and were primarily formwork related.

For example, plywood formwork debris fell from the 29<sup>th</sup> floor in June 2006, striking and injuring a female pedestrian, requiring medical attention. In February 2009, a piece of 3x4 formwork debris fell from the upper floors of a construction site on West 45<sup>th</sup> Street, Manhattan, injuring a flagman.



**Figure B.7.1: Debris Accumulation Presenting a Public and Worker safety Hazard. Note Unprotected and Unsecured Building Edge (Background).**



**Figure B.7.2: Unacceptable Debris Accumulation and Material Storage during Formwork Operations. Lack of Storage Space Concentrates Material within Work Areas, Impeding Egress Pathways. Note Shoring Post (Center) Stopped Short of Floor over Stacked Material.** 



**Figure B.7.3: Stacked and Unsecured Material Presents a Wind Borne Debris Hazard When Placed Near Building Edges** 

Additionally, recommendations regarding New York City's construction inspectors will help establish more consistent DOB inspection procedures and enforcement. As industry complaints regarding inconsistent levels of enforcement are common, recommendations relative to the standardized application of violation thresholds and new low-risk construction practices provide a basis for long term violation reductions.

## **B.7.2 Recommendation HC-8: DOB Inspector Qualifications**

*Enhance level of knowledge among DOB inspectors to include qualifications consistent with current NYC Building Code requirements regarding site safety practices, proper concrete formwork installation, and proper shoring and reshoring placement*.

Inspectors should be required to receive training equivalent to that of safety professionals in the private sector, such as a Certified Safety Professional, NYC Certified Site Safety Manager, Occupational Health and Safety Technologist, or the Construction Health and Safety Technologist, either through DOB-provided education or through external channels<sup>13</sup>.

Increasing the inspector's knowledge base in this manner is critical to maintaining the DOB's credibility within the construction community, allowing them to enforce code requirements with continued authority and consistency. In addition to basic safety practice education, DOB inspectors should be trained to do the following:

- Read and understand formwork design drawings
- Become ACI Level 1 Certified<sup>14</sup>
- Understand the importance of proper shoring sequences and practices
- Quickly Identify and Address Risky Construction Operations

#### **B.7.3 Recommendation HC-9: DOB Inspection Procedures**

*Update and publish standard sets of inspection protocols to create a consistent and uniform level of enforcement*.

A repeated industry criticism of DOB inspection practices is the non-uniform level of enforcement. Updated protocols are to include specific inspection check lists listing thresholds for violations, as well as thresholds for Stop Work Orders.

Current DOB inspection checklists and standard operating procedures (SOP), while specific in reference to many code requirements, do not provide guidelines sufficient to provide for a uniform enforcement of safety-critical requirements. For example, inspectors are currently not uniformly equipped to judge the acceptability of common unsafe conditions (Figs. B.7.4- B.7.7). Rather, they rely primarily on their own varying level of training, experience, and degree of tolerance of non-conforming issues.

<sup>&</sup>lt;sup>13</sup> BCSP Board of Certified Safety Professionals, 208 Burwash Avenue, Savoy, IL 61874.

 $14$  The DOB has already begun to certify inspection staff per ACI Level 1



**Figure B.7.4: Localized Gap Condition at Guardrail. Lack of Specificity Regarding Allowable Gap Distance (if any) Forces Inspector to Make a Potentially Inconsistent Judgment Call** 



**Figure B.7.5: Localized Discontinuous Guardrail Condition at Material Storage Location. Lack of Specificity Regarding Allowable Gap Distances Forces Inspector to Make a Potentially Inconsistent Judgment Call**


**Figure B.7.6: Building Exposure with Incomplete Edge Protection. Code Provisions Do Not Address Violation Thresholds Relating to Percentage of Exposure without Protection** 



**Figure B.7.7: Localized Variation in Guardrail Height. Code Provisions Do Not Address Allowable Height Tolerances (if any). Lack of Specificity Forces Inspector to Make a Potentially Inconsistent Judgment Call** 

An upgraded SOP would benefit greatly from an array of easily-recognizable photographic examples. Explicit SOP inspection protocols and thresholds for violations will eliminate the need for DOB inspectors to exercise personal judgment regarding violations. This revised SOP protocol may include the following model requirements, augmenting and clarifying existing protocol guidelines (Figure B.7.8).

- Maintain less than 6" between discontinuous guardrails and building elements, or between collections of stored material and the resumption of guardrail protection. *Enforcement level: Violation*
- Deflection of guardrail cables shall not exceed  $\frac{1}{4}$ " for every foot of unsupported length (tautness)15. *Enforcement Level: Violation*
- Without Exception, fully compliant guardrails shall be continuously installed throughout building perimeter. *Enforcement Level: Stop Work Order*



#### **Figure B.7.8: Portion of Current DOB Standard Operation Procedure v6**

 $15$  Compare to DOB SOP v6 Section 16 (c), (f)

## **B.7.4 Recommendation HC-10: Housekeeping Requirements**

*Clarify specific housekeeping requirements in inspection protocols<sup>16</sup>*.

Similar to the need to clarify enforcement of guardrail conditions, and in an attempt to reduce the risk of falling debris, a uniform understanding of acceptable housekeeping conditions is required. An upgraded SOP would benefit greatly from an array of easily-recognizable photographic examples (Figures B.7.9-B.7.11).



**Figure B.7.9: Unacceptable Level of Debris Accumulation.** *Enforcement Level: Violation* 

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<sup>&</sup>lt;sup>16</sup> Housekeeping provisions to augment OSHA 29 CFR 1926.25



**Figure B.7.10: Unacceptable Level of Debris Accumulation Presenting a Major Impediment to Egress.** *Enforcement Level: Stop Work Order* 



**Figure B.7.11: Acceptable Level of Debris Accumulation** 

## **B.7.5 Recommendation HC-11: Site Safety Hierarchy (Further Study)**

*Require site safety personnel's line of accountability to lead to owner (and not to the contractor or CM) to avoid a conflict of interest.* 

A precedent for this recommendation is Los Angeles where Site Safety managers are hired directly by the owner. Observations and interviews collected during 181 site visits indicate a Site Safety Manager's ability to maintain appropriate levels of safety on job sites is directly related to the owner's and contractor's willingness to support his efforts. A May, 2004 study<sup>17</sup> found that the Site Safety Personnel's authority level is highly correlated with overall safety. Additionally, current American Society of Civil Engineers (ASCE) policy<sup>18</sup> states that "Owners should take an active role in project safety." Enabling safety personnel to pursue their duties unencumbered by conflicts of interest is an efficient way to achieve increased levels of safety.

Site Safety Managers have a purpose, but are currently ineffectual. Even highlyqualified and knowledgeable safety managers were observed to be ineffective, relative to enacting and enforcing safety compliance, without the contractor's direct support. Because contractors are under significant pressure to adhere to strict construction schedules, they are generally not inclined to delay projects to enforce safety regulations (Figure B.7.12) throughout the construction site. Although cooperation was observed to exist between the General Contractor and Safety Personnel at a number of sites, HRCO team members noted this as the exception rather than the rule.

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<sup>&</sup>lt;sup>17</sup> Benchmark Studies on Construction Safety Management in China. Journal of Construction Engineering and Management

<sup>&</sup>lt;sup>18</sup> ASCE Policy Statement #350 (1998)



**Figure B.7.12: Failure to Tie-off within 10 feet of Unprotected Edge** 

HRCO field note entry of significance regarding excellent safety coordination:

- 1-Oct. 2008, Site No. 23: Owner-hired Site Safety Manager, observed good safety response over contractor hired Site Safety Manager
- 2-Oct. 2008, Site No. 40: Interview with Site Safety personnel indicate preference is to be hired by owner, and owner involvement improves ability to enforce safety regulations.
- 22-Oct. 2008, Site No. 48: Site safety manager observed that they are more successful on project when they are retained by the owner.

HRCO field note entries of significance regarding poor safety coordination:

• 18-Aug. 2008, Site No. 85: Poor chain of command between Site Safety Manager and trades. Lack of respect between trades and safety manager. Site Safety Manager unable to control project, under pressure to keep low profile.

- 27-Aug. 2008, Site No. 90: Limited ability of SSM to maintain control of site. Housekeeping violations and unprotected edge violations previously issued by BEST.
- 24-Sept 2008, Site No. 55: Additional concrete contractor safety personnel onsite, but ineffective.
- 25 Sept. 2008, Site No. 57: Site Safety personnel not effective in maintaining safety. Insufficient perimeter protection. Unprotected edges throughout site. Poor housekeeping
- 21-Oct. 2008, Site No. 56: General contractor slow to address safety issues. Lack of fall protection between buildings. Fall hazards at ladders to stripping floor (Safety violations issued following week following deteriorating conditions).
- 23-Oct. 2008, Site No. 85: Site Safety Manager ineffective. Unprotected edges throughout. Most workers not tied off. No safety coordination or enforcement within project team.
- 5-Nov. 2008, Site No. 85: Site Safety Personnel have no control over site safety. Still inadequate edge protection. No tie off compliance. Blocked egress. Project team is not making safety a priority.

## **B.7.6 Recommendation HC-12: Upgrading Netting Requirements (Further Study)**

*Study the effectiveness of enhancing existing netting requirements*19.

Current NYC construction industry practice regarding formwork construction relies heavily upon the use of site constructed dimension lumber (stick) assemblies (Figure B.7.13), consisting of timber posts and lumber framing members which typically create large volumes of waste and debris. In recognition of the likelihood that this debris represents a potential hazard, and the further recognition of the potentially serious hazards created if the debris is blown or falls from a building, a number of general contractors have independently elected to utilize full-height vertical netting (Figure B.7.14) to better contain flying debris, in excess of current DOB code requirements.

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 $19$  Netting Provisions to augment OSHA 29 CFR 1926.502 and 1926.750

As the industry begins to independently move in the direction of more stringent netting requirements, and while public safety remains a high priority, a review of current standards is necessary.



**Figure B.7.13: Typical Site Constructed Dimensional Formwork Assembly (Stick Form Construction)** 



## **Figure B.7.14: Full-height Vertical Netting Provides Additional Barrier to Flying Debris**

Further study of cocoon construction practices (Figure B.7.15), which can contain debris more effectively than full-height netting alone, is also warranted. When correctly implemented, cocoon configurations provide protection against worker fall incidents by allowing construction to proceed within an enclosed temporary structure encircling the building footprint. Consideration must be given however, to the cocoon system's effect on fire safety, wind design and egress.



**Figure B.7.15: Cocoon Construction in Operation.** 

## **B.7.7 Recommendation HC-13: Material Handling (Further Study)**

*Establish requirements for the use of outrigger systems for material handling*.

Outrigger platforms are temporary structures cantilevered off building edges (Figures B.7.16-B.7.17) that can be constructed to provide a continuously-protected material rigging area outside the building footprint. Incorporation of outrigger platforms into the construction scheme will eliminate the need to interrupt otherwise continuous edge protection, allowing rigging and flying operations to proceed in a protected environment<sup>20</sup>. Additionally, outrigger systems, located and installed at specific locations on each floor, will eliminate subjecting crane booms to lateral loads when material is dragged out of the building interior prior to lifting the load (see also HRCO Crane Rigging Recommendation to restrict the practice of "side pulling" loads).

<sup>&</sup>lt;sup>20</sup> Outrigger systems to comply with OSHA 29 CFR 1926.452(i). Designs to be stamped and sealed by a registered NY Professional Engineer



**Figure B.7.16: Acceptable Outrigger System for Material Handling Near Ground Level. Note Uninterrupted Edge Protection.** 



**Figure B.7.17: Acceptable Outrigger System for Material Handling Near Active Floors (Top)** 

The 2008 New York City Building Code §3303.4.5.2 allows material to be stored while overhanging building edges provided they are sufficiently banded and braced. Although instances of code non-compliant material handling and storage practices were rare, concerns were raised regarding the potential of the current practice of material handling and storage to cause a serious incident or accident either through rigging errors, or by creating serious fall hazards (Figure B.7.18).

Also, HRCO site observations confirm that code-compliant placement and rigging of material at building edges occurs coincidentally with code non-compliant removal of edge protection (Figures B.7.19-B.7.20). Thus, edge protection is removed, creating a code non-compliant condition, to allow for the code-compliant practice of placing material at the building edge for lifting to overhead floors.

The HRCO has not identified any typical construction logistics that would preclude the use of outriggers. However, implementation of this recommendation may be benefited by providing a mechanism for contractors to elect not to use out-riggers either by special filing or for certain classes of buildings.



**Figure B.7.18: Typical Unacceptable Lack of Edge Protection at Building Edge Coincident with Material Storage. Guardrails Removed over a Large Portion of This Building's Exposure to Accommodate Material Piles** 



**Figure B.7.19: Current Code-Compliant Material Storage Practice (Piled Material is Banded and Braced) and Accompanying Fall Hazard at Unprotected Edge (Left)** 



**Figure B.7.20: Hoisting of Debris Container (Mini) Requires Rigging Operations at Unprotected Edge. Hoisting Will Also Require Crane "Side-Pulling". Note Lack of Proper Worker Tie-Off** 

## **B.7.8 Additional HRCO Data**

## **B.7.8.1. Construction Schedule Analysis and Violation Issuance Analysis**

Two analyses were conducted to evaluate the effectiveness of violation issuances on construction quality and safety issues, and whether there is a statistically significant correlation between the frequency of violations and construction cycle time.

In summary, analysis indicates that issuing a violation has no effect on general code compliance or prevention of violation recurrence. Analysis also concluded that although construction sites with quick construction schedules are likely to contain hazardous housekeeping conditions, these same sites are not any more likely to contain hazardous safety or quality conditions than sites with slow construction schedules.

## **Construction Schedule Analysis**

For the purposes of the HRCO study, violation categories are defined as follows:

• Housekeeping Violations: Instances where significant levels of debris accumulation exist, presenting a hazard to egress or production of falling material.

- Unprotected Edge Violations: Instances where leading edge or interior fall hazards are not properly secured per New York City code requirements. Items such as missing railings, loose fence cables, and exposed edges are considered violations.
- Tie-off Violations: Refer to instances where OSHA guidelines regarding proper Personal Fall Arrest System (PFAS) usage have been violated. Violations include failure to tie off within ten feet of an unprotected edge and failure to secure lanyards to adequate anchorage points.
- Formwork Non-Compliance: Instances where formwork design or construction creates a significant hazard to worker or public safety $2^1$ .
- Construction Quality Violations: Instances where constructed conditions are out of compliance with approved design or accepted NYC building code requirements.

The number of violations as a function of construction cycles (days) was evaluated. The construction cycle data collected by the HRCO and listed in Table 1 were analyzed to determine statistical trends between the percentage of violations and construction cycle time (construction schedule).



## **Table 1: Construction Cycle Data Summary**

<sup>&</sup>lt;sup>21</sup> See High Rise Concrete Formwork Recommendations

### **Correlation**

Analysis was performed to calculate the sample correlation coefficient, r, between the percentage of violations and construction cycle (days) for each violation category. This coefficient varies between -1.0 (perfect negative linear correlation) to 1.0 (perfect positive linear correlation). A correlation coefficient of 0 implies no correlation between the percentage of violations and construction cycle. Correlation coefficients ranged from -0.882 (negative linear correlation for "Housekeeping") to 0.272 (positive linear correlation for "Unprotected Edges").

Hypothesis testing was conducted using the sample correlation coefficient to determine if the population correlation coefficient, ρ, was significantly different from 0. With the exception of the "Housekeeping" category, the null hypothesis that there is no linear association between the percentage of violations and construction cycles can not be rejected at the 5% level of significance.

Hypothesis testing was next conducted using the sample correlation coefficient to determine if the population correlation coefficient, ρ, for the "Housekeeping" category was negative. The null hypothesis that there is no linear association between the percentage of "Housekeeping" violations and construction cycles was rejected at the 5% level of significance indicating that there is a strong negative correlation (e.g. the percentage of housekeeping violations decreases with an increase in construction cycle times).

Based on the correlation analysis the null hypothesis of no population correlation between construction cycles and "Housekeeping" violations can be rejected at the 5% level of significance, strongly suggesting the hypothesis of negative linear correlation.

In conclusion, there is no significant evidence of correlation between construction cycles and the percentage of "Unprotected Edges", "Worker Not Tied Off", "Formwork Non-Compliance", and "Construction Quality" violations observed during the HRCO's summer 2008 site observations

### **Rank Correlation**

The correlation analysis above was conducted on a relatively few number of data points (construction cycles ranging from 2 through 7 days). Statistical inference that the percentage of "Housekeeping" violations decreases with increased construction cycle days assumes that observations are sampled from a joint normal distribution and that there are no extreme observations.

A rank correlation analysis (less susceptible to the influence of extreme values) was conducted for each construction cycle category to test the null hypothesis that there is no

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association between the percentage of violations and construction cycles. Data were first ranked in ascending order and the Spearman's rank correlation coefficient was computed from the rankings.

Hypothesis testing was conducted using Spearman's rank correlation coefficient to determine if there is a correlation (positive or negative) between the rankings of violation percentages with construction cycles. The null hypothesis that there is no linear association between the ranked percentage of violations and construction cycles can not be rejected at the 5% level of significance. Based on the rank correlation analysis hypothesis testing, there is no statistically significant correlation (5% level of significance) between the ranking of each violation category percentage and construction cycle.

## **Conclusions**

Two types of correlation analyses were conducted to evaluate whether there is a statistically significant sample correlation coefficient, r, between the percentage of violations and construction cycle times for each type of violation category.

The correlation analysis assumed that observations are sampled from a joint normal distribution and that there are no extreme observations. The null hypothesis of no population correlation between construction cycles and "Housekeeping" violations can be rejected at the 5% level of significance and suggests strong evidence supporting the hypothesis of negative linear correlation (decrease in the percentage of "Housekeeping" violations with an increase in construction cycle times). *There is no significant evidence of correlation between construction cycles and the percentage of Unprotected Edges, Worker Not Tied Off, Formwork Non-Compliance, and Construction Quality violations.*

## **B.7.8.2. Effect of Heightened Enforcement**

In addition to the HRCO's standard safety observation protocol (for which jobsites were selected by a standard procedure discussed in the high-rise concrete methodology section of this report), a select group of sites was chosen to receive additional scrutiny to assess the effect of repeated enforcement. Violation timeline data were analyzed to evaluate effects of heightened enforcement and violation issuances for the following sites:

- Site No. 85, Brooklyn
- Site No. 84, Manhattan
- Site No. 56, Manhattan

• Site No. 57, Manhattan

Violation category data culled from HRCO site visits (Figures B.7.21-B.7.24) were rated as "Satisfactory", "Unsatisfactory, No Violation Issued", "Unsatisfactory, Violation Issued" and, "Stop Work Order in Effect" in Table 2.

A greater percentage of the visits with "Unsatisfactory" ratings (with or without violations issued) or stop work orders is reported for the "Formwork Compliance" (85%) and "Construction Quality" (86%) categories.





### **Effect of Violations**

Timeline data were evaluated to determine the effect of violations. As summarized in Table 3, the number of visits to achieve a "Satisfactory" rating averaged 2.7 visits when no violations were issued and 3.0 when violations were issued. On average, issuing violations did not decrease the number of visits to achieve a "Satisfactory" rating.

A contingency table analysis was conducted to evaluate whether there was an association or dependence between the number of repeat visits to achieve a "Satisfactory" rating and violation issuance. The "Unsatisfactory" data with or without violations were first classified as "acceptable" if a "Satisfactory" rating was achieved in one to two repeat visits or "unacceptable" if achieved in three or more visits. Data were also cross-classified by whether violations were issued or not. The cross-classified data are summarized in Table 4.



### **Table 3 – Number of Repeat Visits**

**Table 4 – Violations Issued Contingency Table** 

	<b>Number of Visits to "Satisfactory"</b>										
		1 to $2$	3 or More								
	<b>Actual</b>	<b>Expected</b>	<b>Actual</b>	<b>Expected</b>	Total						
<b>No Violation</b>	34	30.8	23	26.2	57						
<b>Violation</b>	12	15.2	16	12.8	28						
Total	46		39		85						

Hypothesis testing was conducted to determine if there are statistical differences between the actual and expected number of visits in the four categories of Table 4. The null hypothesis that there is no linear association between the actual and expected number of visits to achieve a "Satisfactory" rating was rejected at both the 5% and 10% level of significance, indicating that there is no statistical evidence that violations are associated with the number of visits. *Issuing a violation has no effect on reducing the number of visits to achieve a "Satisfactory" rating.* 

### **Moving Forward**

This study is limited to four sites over a limited time period. Consequently, additional investigation may be warranted to gage the effect of increased enforcement (especially stop work order efficacy). Further investigation may be performed as outlined in the following procedure.

- 1. Select five sites with a history of safety violations for additional scrutiny within five subject categories: Unprotected edges, Worker Tie-off, Housekeeping, Formwork Compliance and Construction Quality.
- 2. Confirm violation thresholds for the five subject categories, for example, establish pictorial reference standards for acceptable levels of housekeeping debris.
- 3. Visit each site as noted below and issue violations and stop work orders when warranted, but with a zero-tolerance policy towards infractions. For example, stop work orders for debris accumulation must still be issued even if workers were "in the process of addressing the issue".



### **Table 5: Reinspection Frequencies**

- 4. Assess performance over a two-month period.
- 5. Sites with improved levels of compliance may be audited monthly to ascertain levels of continued compliance.
- 6. Continued, repeat non-compliance indicates insufficient deterrent levels, warranting the DOB's reevaluation of penalties. Increased violation fees and mandatory stop work orders may be effective in increasing compliance levels.



**Figure B.7.21: HRCO Condition Report Timeline at Site No. 85, Brooklyn. Note Appearance of New Controlled Inspector and Lather Crew on 18-Sep.** 

Issue	ခြံချီချီချီချီ မြစ်မြစ်မြစ် ခြံခြံခြံခြံ			
BEST Inspector Present?	Y			
Unprotected Edges				
Worker Tie Off				
Housekeeping				
Formwork Compliance				
<b>Construction Quality</b>		X		
Stop Work Order				
Notes:				
Stop Work Order Issued Independer 1.				
Stop Work Order Issued for Imprope 2.				
Legend:			Satisfa	
			Unsati:	
			Unsati:	
			Stop V	
	X		Violatio	

**Figure B.7.22: HRCO Condition Report Timeline at Site No. 84, Manhattan** 

Issue	3-Aug		$\frac{1}{2}$	
BEST Inspector Present? N		Υ		
Unprotected Edges		X		
Worker Tie Off				
Housekeeping				
Formwork Compliance				
<b>Construction Quality</b>				
Stop Work Order				
Notes:				
Stop Work Orders Issued for Inadequ 1.				
Stop Work Orders Issued for Inadequ 2.				
Legend:			Satisfa	
			Unsatis	
			Unsatis	
			Stop W	
	$\overline{\mathbf{x}}$		Violatio	

**Figure B.7.23: HRCO Condition Report Timeline at Site No. 56, Manhattan** 



**Figure B.7.24: HRCO Condition Report Timeline at Site No. 57, Manhattan** 

## **B.8 WORKER FALLS**

## **B.8.1 Description**

The High Risk Construction Oversight (HRCO) High-Rise Concrete Team observed significant numbers of safety hazards involving missing or misuse of required fall hazard protection, including tie-off safety practices (Table 1).

Existing fall-prevention requirements (edge protection, tie-offs, etc.) are currently included in the NYC Building Code and Federal OSHA CFR 1926.500 regulations. Code provisions are sufficient to mitigate these hazards; however, the provisions are routinely ignored and/or violated.

HRCO High-Rise Concrete Team observations indicate, in general, a worker's lack of basic tie-off knowledge. This lack of knowledge is typically coupled with a reluctant attitude, on the part of the worker, to comply with personal safety regulations and a relaxed approach, on the part of the contractor, to enforce proper fall protection regulations at the site. This lax attitude, on the part of the individual worker, is exacerbated at construction sites where the Site Safety Personnel's line of accountability inhibits proper enforcement of safety regulations, or where the project team does not provide the support required to execute proper safety protocols.

	<b>All Active Projects</b>
<b>Number of Site Observations</b>	181
<b>Unprotected Edges</b>	78 (43%)
<b>Tie-off Non-compliance</b>	57 (31%)

**Table 1: HRCO Observed Fall Violations** 

Preventing fall hazard conditions, such as those during formwork operations (Figure B.8.1) can be accomplished with minimal cost when the contractor consciously anticipates safety solutions. In the case of typical site constructed dimension lumber<sup>22</sup> (stick) form assemblies, proper lanyard anchor points can be built into the formwork substructure and access ports for lanyards can be integrated into decking systems. The use of retractable lanyards (Figure B.8.2) can then provide adequate worker mobility throughout the entire deck area until proper guardrails are fully installed.

 $\overline{a}$ 

 $22$  Typically consisting of timber posts and lumber framing members

Proper implementation of adequate OSHA and New York City Building Code compliant tie-off and edge protection practices is both realistic and achievable with current technology (Figures B.8.3- B.8.4). The cost of investment in equipment and training is insignificant in comparison to the cost of lost productivity after a preventable accident occurs. A HRCO field note entry of significance regarding existing stick form tie-off coordination practices:

• 27-Oct. 2008, Site No. 72: Tie-off anchorages used on forming floor, pulled through holes in decking.



**Figure B.8.1: Failure to Tie-off During Decking Operations. Retractable Lanyards Could Have Been Utilized, Anchoring to Formwork Subassembly** 



### Miller 10 Ft Retractable Webbing Lanyard with Carabiner

Get maximum fall protection with Miller's 10 Ft Retractable Webbing Lanyard with Carabiner Item #: A504-6190 Manufacturer: Sperian Protection - Miller Fall Protection<br>Manufacturer: Sperian Protection - Miller Fall Protection Product Type: Fall Protection

**Figure B.8.2: Retractable Lanyard** 



**Figure B.8.3: Proper Tie-off. Note Use of Built-in Anchor Points on Engineered Formwork (Prefabricated Steel) Towers** 



**Figure B.8.4: Tie-off to Formwork Substructure Using Retractable Lanyard** 

## **B.8.2 Recommendation HC-14: Fall Hazard Awareness**

*Implementation of a fall hazard awareness campaign through the use of posters, ads, and training at each jobsite for workers before they are allowed on site.* 

Worker falls at construction sites account for more fatalities than any other cause<sup>23</sup> (Table 2), thus any change in fall rates will have a significant impact upon fatality reduction. Continued implementation of the DOB's current fall hazard awareness campaign will be relied upon to positively effect changes to worker attitudes towards fall prevention. Similar OSHA awareness programs were able to cut fatal trenching incidents by half over a four year period.

<sup>&</sup>lt;sup>23</sup> Nationwide, the Bureau of Labor Statistics attributes 442 of 1,178 (38%) construction fatalities to falls

	<b>Incident</b>	<b>Accident</b>	<b>Injuries</b>	<b>Fatalities</b>
All Causes, All	1133	321	389	49
<b>Categories (Concrete)</b>	(132)	(58)	(63)	(6)
<b>Worker Fell, All</b>	182	166	151	27
<b>Categories (Concrete)</b>	(31)	(28)	(26)	(4)
Worker Fell as % of All <b>Causes</b> (Concrete)	16.1% (23.5%)	51.7% (48.3%)	38.8% (41.3%)	55.1% (66.7%)

**Table 2: Historical DOB Accident-Incident Data. 2-January 2006 to 30-June 2008** 



**Figure B.8.5: Current NYC DOB Fall Awareness Poster** 

## **B.8.3 Recommendation HC-15: Contractor Documentation (Further Study)**

*Require contractor to document remedial actions taken when workers are identified as non-compliant regarding safety measures, including tie-off requirements. Remedial actions could include additional training sessions, suspension, or removal from job site.* 

Contractors and onsite safety team members are best equipped to identify and rectify fall hazard issues (Figure B.8.6). Furthermore, these individuals have the most at stake when an accident occurs. Therefore, conscious recognition and acknowledgement of remedial actions on the part of the contractor are warranted.



**Figure B.8.6: Commonly Observed Failure to Tie-off During Formwork Erection Operations** 

### **B.8.4 Recommendation HC-16: Repeat Offense Enforcement (Further Study)**

*Require a "two strikes and you're out" provision to be levied against the contractor in the event the contractor fails to enforce safety regulations and procedures. This clause would require that the project is shut down a prescribed number of days after a predetermined number of code violations or reportable incidents. The purpose of the shut down is to provide the contractor a period of time to properly implement safety measures.* 

The threat of DOB-issued violations for code violations, such as poor housekeeping and improper tie-off procedures presenting a hazard to the public was found to be insufficient to ensure conformance to safety requirements. Also, repeat offenses are common (Figures B.8.7- B.8.9).



**Figure B.8.7: Initial Failure to Tie-off at Site No. 86, 3-Sept. 2008 (OSHA Violation)** 



**Figure B.8.8: Repeat Failure to Tie-off at Site No. 86, 10-Sept. 2008 (OSHA Violation)** 



**Figure B.8.9: Repeat Failure to Tie-off at Site No. 86, 24-Nov. 2008 (OSHA Violation)** 

For example, Figure B.8.10 summarizes OSHA tie-off violations observed by the HRCO between August and November of 2008. The Department of Buildings' issuance of violations in cases where tie-off conditions presented a hazard to public safety (see 30-October entry) had limited effect on subsequent code-compliance<sup>24</sup>.



**Figure B.8.10: Repeat Tie-Off Violation History, Site No. 85** 

Observations and interviews with construction team members, including contractors, site safety personnel, and DOB inspectors, confirm that violation fees are considered a "cost of doing business", and that the single most effective enforcement method is a stop work order. The DOB may elect to strengthen this recommendation by requiring site shut down after only one observed incidence of all types of fall hazard non-compliance (edge protection, tie-off, etc...)

<sup>&</sup>lt;sup>24</sup> See General Site Safety Recommendations for additional analysis and discussion

## **B.9 SPECIAL INSPECTION AND CONSTRUCTION QUALITY**

## **B.9.1 Description**

The High Risk Construction Oversight (HRCO) High-Rise Concrete Team documented numerous instances of the fabrication and installation of reinforcing steel that did not comply with code requirements or industry standards. Furthermore, the HRCO High-Rise Concrete Team has observed numerous instances of inadequate and/or inconsistent inspection of installed reinforcing steel.

Of the 98 active site observations completed by HRCO engineers, forty-nine percent (49%) contained construction defects. Construction defects include New York City Building Code violations, violations of the *Building Code Requirements for Structural Concrete,* (ACI 318), and work that did not comply with the structural design drawings and/or the approved shop drawings. Deficient conditions broadly include the following:

- Improper bar placement
- Improper bar fabrication
- Ineffective special inspection

Although the HRCO site observation program noted many instances of low quality bar fabrication and placement, proper procedures were observed in New York City at both Union and Non-Union worksites. Knowledge resources such as the Lathers Union's Queens training facility actively promote industry best practices and code-compliant installations.

## **B.9.2 Recommendation HC-17: Special Inspection Rule**

*Strengthen outreach to industry on Special Inspection qualifications, and enforce the requirement that all Special Inspectors are properly registered and/or certified in compliance with NYC Special Inspection Rule requirements, effective July 1, 2009*.

Based on HRCO observations, the percentage of structures found to contain critical construction defects (Tables 1-2, Figs. B.9.1-5), despite direct oversight in each case by a controlled inspector<sup>25</sup>, supports the actions previously taken by the DOB to improve special inspector expertise. In light of actions taken by the DOB, concerns have been raised by construction industry leaders regarding the industry's ability to provide adequate numbers of properly-qualified inspectors prior to the July 2009 deadline. Therefore the DOB's industry outreach will be critical in ensuring a smooth transition to the new inspector requirements.



### **Table 1: HRCO Construction Quality Defect Rate**

<sup>&</sup>lt;sup>25</sup> Now "Special Inspector" under The 2008 NYC Building Code






**Figure B.9.1: Typical Critical Quality Defect: Column Splices Noncompliant with ACI. Conditions Subsequently Remedied to the Satisfaction of the Engineer of Record** 



**Figure B.9.2: Typical ACI-Compliant Splice Detail** 



**Figure B.9.3: Typical Critical Quality Defect: Improper Shear Stirrup Engagement. Conditions Subsequently Remedied to the Satisfaction of the Engineer of Record** 



**Figure B.9.4: Typical Critical Quality Defect: Bar Congestion and Improper Shear Stirrup Engagement. Conditions Subsequently Remedied to the Satisfaction of the Engineer of Record** 





#### **B.9.3 Recommendation HC-18: Field Inspection**

*Enhance level of knowledge among DOB inspectors to include qualifications consistent with the current NYC Building Code (Table 3), specific to ACI Special Inspector training, to promote consistent enforcement of concrete practices, including field testing procedures.* 

Currently, DOB inspectors generally lack sufficient training to consistently enforce critical quality issues. This is because there is no standard training procedure in place that addresses these types of issues. To appropriately enforce critical DOB construction quality code requirements, inspectors must possess a sufficient level of knowledge of the material at hand, and meet or exceed the special inspector's level of expertise in the field.

The Department of Buildings has already taken steps to certify BEST inspectors as ACI Level-1 Technicians. This education will allow inspectors to better assess the performance of field personnel responsible for sampling and approval of freshlydelivered concrete. Furthermore, ACI Level-1 training is a prerequisite to enroll in the Concrete Construction Special Inspector Program. This program covers topics

critical to proper steel placement, such as tolerances, and topics critical to proper concrete consolidation.

#### **Table 3: DOB Inspector Qualifications to Match Requirements for Special Inspectors, NYC BC 1627**



#### **B.9.4 Recommendation HC-19: Inspection of Testing Labs**

*Enhance level of knowledge among DOB personnel to include qualifications consistent with the current NYC Building Code (Table 3), specific to ACI Special Inspector training, and other similar certifications to promote consistent inspection of laboratory practices and conditions.* 

Training of DOB personnel consistent with this recommendation is critical regarding the DOB's continued, periodic auditing of concrete testing laboratories for quality and code compliance. HRCO inspections have shown that laboratory quality is highly variable, with each laboratory displaying at least some level of nonconformance with code-required testing procedures (see section B.3.2). Additionally, as the DOB will require testing laboratories to obtain AASHTO $^{26}$ accreditation by July of 2010, it will be necessary for the DOB knowledge base to

<sup>&</sup>lt;sup>26</sup> American Association of State Highway and Transportation Officials

remain current with AASHTO requirements through education and training programs.

#### **B.9.5 Recommendation HC-20: Reinforcing Bend Quality Assurance**

*Require documentation through photo and/or video that site bending practice complies with accepted industry standards and tolerances. Conformance may be spot checked by the DOB through inspection of logs and field conditions.* 

HRCO engineers observed numerous instances of fabricated reinforcing that did not conform to industry standards<sup>27</sup> as dictated by The New York City Building Code (Figures B.9.6- B.9.7). A failure of the construction industry to provide quality bar fabrication resulted in this recommendation since improper bar fabrication is likely to introduce critical structural defects.

Augmentation of the special inspector's existing daily reporting documents to include photo documentation of proper and consistent bend quality would allow the Department of Buildings to verify that best bending practices in conformance with code requirements are being utilized regularly. Without this type of documentation (and without constant observation by a DOB inspector), the DOB will be unable to confirm that improved procedures are being enacted.

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<sup>&</sup>lt;sup>27</sup> Specifically American Concrete Institute (ACI) Requirements



**Figure B.9.6: Improperly Fabricated Shear Stirrups, Resulting in Improper Stirrup Engagement. Conditions Subsequently Remedied to the Satisfaction of the Engineer of Record** 



**Figure B.9.7: Bar Fabrication Noncompliant with ACI28. Conditions Brought to the Attention of the Engineer of Record** 

### **B.9.6 Recommendation HC-21: Reinforcing Placement Quality Assurance**

*Require documentation through photo and/or video that steel placement complies with accepted industry standards and tolerances. Conformance may be periodically spot checked by the DOB through inspection of construction logs and field conditions.* 

HRCO engineers observed numerous instances of installed reinforcing that did not conform to the design documents, the approved shop drawings, or industrystandard code requirements (Figures B.9.8- B.9.10). A failure of the construction industry to monitor, install, and provide quality bar placement resulted in this recommendation since improper bar placement and installation will likely introduce structural defects, some of which may be critical.

<sup>&</sup>lt;sup>28</sup> Bend Radius is Tighter than Allowed by American Concrete Institute (ACI) Specifications

The justification to augment the special inspector's existing daily reporting documents to include photo and/or video documentation of bar placement is twofold. One, the Department of Buildings will be able to verify upon review of the documentation that bar placement is in conformance with code requirements (without the need for constant on-site observation by a DOB inspector); and, two, the documentation will allow review of constructed assemblies by design professionals if placement questions arise.



**Figure B.9.8: Lack of Proper Shear Stirrup Engagement. Condition Soon to be Hidden by Concrete Encasement. Conditions Brought to the Attention of the Engineer of Record** 



**Figure B.9.9: Column Bar Congestion. Conditions Brought to the Attention of the Engineer of Record** 



**Figure B.9.10: Severe Bar Congestion29. Conditions Brought to the Attention of the Engineer of Record** 

<sup>&</sup>lt;sup>29</sup> American Concrete Institute Specifications Require Minimum Spacing Between Bars, Greater of One Inch or Diameter of Bar to Allow for Proper Concrete Consolidation

### **B.9.7 Additional HRCO Data**

<b>Address</b>	<b>Boro</b>	<b>Notes</b>	
3	$B3^{30}$	Insufficient stirrup Engagement.	
$\overline{4}$	$B1^{31}$	Insufficient stirrup engagement	
14	<b>B1</b>	Insufficient stirrup engagement. Bar Congestion	
14	<b>B1</b>	Improper hook fabrication	
15	<b>B1</b>	Insufficient stirrup engagement. Improper column tie fabrication and installation	
45	<b>B1</b>	Improper Splice Configurations, Improper Bending of Embedded Steel	
48	<b>B1</b>	Improper Splice Configurations, Improper Bending of Embedded Steel. Bar Congestion	
55	<b>B3</b>	Insufficient Column tie engagement. Improper hook fabrication. Improperly placed column bars	
67	<b>B1</b>	Improper Splice Configurations, Improper Bending of Embedded Steel	
72	B1	Improper Splice Configurations, Improper Bending of Embedded Steel	
72	<b>B1</b>	Improper stirrup Engagement	
74	<b>B1</b>	Bar Congestion. Insufficient stirrup engagement. Improper column bar placement. Improper splice configurations	
84	<b>B1</b>	Improper Splice Configurations. Insufficient stirrup engagement	
84	<b>B1</b>	Improper Splice Configurations, Improper Bending of Embedded Steel	

**Table 4: Sites with Critical Quality Defects** 

<sup>30</sup> Borough of Brooklyn

<sup>31</sup> Borough of Manhattan



#### **B.9.8 Impact of Construction Quality Deficiencies**

Proper construction and inspection procedures will significantly improve construction quality related to load carrying capacity of structural members. Defects in construction quality may remain unrealized for years or decades as the applied load is generally less than the design load. However, it is likely that a critical loading event could occur during the life of the structure resulting in distress or collapse (e.g. wind loads from a major hurricane). An example to justify the need for proper inspection oversight is illustrated below.

- On 25-September, 2008, HRCO staff observed three, second floor transfer girders with ACI-noncompliant shear steel engagement**<sup>32</sup>** (Figure B.9.11). As constructed, only two of the six shear stirrup legs at the beam soffit were properly hooked around longitudinal reinforcement. Preliminary calculations indicate this bar configuration would have resulted in a 33% reduction in beam shear capacity. This reduced shear capacity could have resulted in serviceability and/or durability issues or, possibly structural failure. A DOB stop work order was put in place until the beams were certified complete and corrected to the satisfaction of the engineer of record.
- Although an initial review of shop and design drawings confirmed sufficient numbers of bottom longitudinal bars, the contractor missed drawing notes requiring the anchorage of all shear hooks with additional steel. A properly trained special inspector would likely have identified not only the noted additional steel requirements, but easily brought the readily-observable code noncompliant conditions to the attention of the contractor and engineer.

<sup>32</sup> ACI-318 §12.13.2.1



**Figure B.9.11: Second Floor Transfer Girder with Improperly Developed Shear Reinforcing. Site No. 47** 

- The same site was visited on 10-October, 2009 and the girder configurations were compared to the stamped design drawing. At this time HRCO staff noted two second floor transfer girders with insufficient numbers of installed shear stirrup sets (Figure B.9.12), bar congestion (Figure B.9.13), and insufficient numbers of installed longitudinal beam top bars. Of the specified 67 sets of shear reinforcement, only 47 sets were installed. Similar to the prior incident, a stop work order was put in place by the DOB until corrective actions could be taken to the satisfaction of the Engineer of Record. Preliminary calculations indicate that shear capacity resulting from this configuration was reduced by 20%. Furthermore, the combined effects of both the September and October defects would have resulted in a shear capacity loss of 44% had these conditions not been remediated.
- Again, it is likely a properly trained special inspector would have identified the egregious lack of sufficient numbers of reinforcing bars, and brought this condition to the attention of the contractor and engineer.



**Figure B.9.12: First Floor Transfer Girder with Insufficient Numbers of Installed Shear Reinforcing Sets. Site No. 47** 



**Figure B.9.13: First Floor Transfer Girder Bar Congestion. Site No. 47** 

### **B.10 PLAN REVIEW**

#### **B.10.1 Description**

The High Risk Construction Oversight (HRCO) High-Rise Concrete Team reviewed a number of construction document sets containing structural engineering drawings that had been submitted to the DOB as part of the permitting process. Furthermore, HRCO team members performed a review of the existing NYC Building Code provisions pertaining to construction document and peer review requirements.

Review of construction documents identified structural design drawings containing incomplete information according to generally accepted industry standards such as American Concrete Institute (ACI) document entitled *Building Code Requirements for Structural Concrete,* ACI 318, ACI document entitled *Details and Detailing of Concrete Reinforcement*, ACI 315 and the *Manual of Standard Practice* published by the Concrete Reinforcing Steel Institute. Incomplete drawing information severely hampers both the construction and peer review processes, is potentially indicative of a substandard level of quality of the structural design work, and could potentially lead to structural integrity and life safety issues in the constructed building.

To the extent that many jurisdictions outside New York City practice high levels of structural design review, the precedent for increased levels of oversight has been established. Responses to the HRCO's benchmark survey (Table 1) suggest New York City's adoption of more stringent plan review criteria would be in line with other building departments nationwide.

<b>Respondent</b>	Percentage of <b>Major Projects</b> Subjected to <b>Detailed Structural</b> <b>Review</b>	Percentage of <b>Major Projects</b> <b>Subjected to Partial</b> <b>Structural Review</b>
<b>Boston</b>		100
Chicago	99	
<b>Fairfax County</b>		100
<b>Honolulu</b>		100
<b>Los Angeles</b>	100	
Philadelphia	100	
San Diego	100	
<b>San Francisco</b>	100	
San Jose	100	
<b>Seattle</b>		100
Toronto	33	90

**Table 1: Plan Review Practices** 

#### **B.10.2 Recommendation HC-22: Monitoring of Peer Review**

*Retain professional engineers on behalf of DOB to monitor that peer reviews of identified projects are properly conducted as required by the NYC Building Code.* 

Peer review, by an independent structural engineer, is an essential component of the design and construction process and is standard practice in many jurisdictions. A majority of major buildings<sup>34</sup> may qualify for peer review under the current criteria<sup>35</sup> contained in the NYC Building Code. This criteria includes, in part:

- 1. Buildings in Occupancy Category IV or more than 50,000 SF of framed area.
- 2. Buildings with aspect ratios of seven or greater
- 3. Buildings greater than 600 feet in height or more than 1,000,000 SF gross floor area

-

<sup>&</sup>lt;sup>33</sup> Remaining 10% Self Certified by Design Professional

<sup>&</sup>lt;sup>34</sup> 2008 NYC Building Code BC 3310

<sup>&</sup>lt;sup>35</sup> 2008 NYC Building Code BC 1627

- 4. Buildings taller than seven stories where any element supports in aggregate more than 15% of the building area
- 5. Buildings designed with non-linear analysis
- 6. As requested by the Commissioner

The identification of structures qualifying for peer review under requirements of BC 1627 requires a structural engineering background, and the number of structures that qualify for peer review may be significant. Therefore, at least one full-time, qualified structural engineer working either on staff or on behalf of the DOB will be required to oversee peer review work. This oversight should include the following:

- Positive identification of structures meeting thresholds for peer review.
- Monitoring of peer review submission procedures.
- Periodic auditing of completed peer reviews for quality and completeness

In addition, the DOB may elect to develop programs for identification of critical structural members not currently addressed in BC 1627 for review, and screening of projects submitted for plan examination approval to prioritize for structural plan review.

#### **B.10.3 Recommendation HC-23: Structural Drawing Information**

*Require minimum level of information to be included on structural building drawings, including member end reactions and details with sufficient information to properly convey the design intent.*

Current DOB plan review procedures do not include technical review sufficient to identify adequacy as prescribed by the NYC Building Code. Furthermore not all sets of structural drawings contain sufficient levels of design information.<sup>36</sup> In addition to existing requirements, and in order to facilitate the peer-review process, the following additional information should be required.

- Member end reactions, including flexure, shear, and axial reactions will be noted on the structural drawings for major structural members such as transfer girders, beam girders, and shear walls.
- Details, and detailing, consistent with ACI 315, Part A

-

<sup>&</sup>lt;sup>36</sup> 2008 NYC Building Code BC 1603 and BC 106.7

• Sufficient notes and details to properly convey the design intent.

#### **B.10.4 Recommendation HC-24: Monitoring of Structural Information Quality**

*DOB should retain professional structural engineers to review drawings to verify that the minimum level of structural information is contained on each set of structural drawings, shop drawings, and formwork drawings. Information to include requirements contained in ACI publications as noted in current NYC Building Code.* 

The volume of plan submissions is significant; therefore, a monitoring program supervised by at least one qualified, full-time structural engineer with sufficient practical design experience is warranted. This program is warranted based on practices in major municipalities (Table 2). While this review is best executed by the owner, the City of New York should maintain sufficient in-house resources to audit a percentage of completed reviews.



#### **Table 2: Engineering Staff**

#### **B.10.5 Recommendation HC-25: Monitoring Constructability**

*DOB should retain professional structural engineers to audit and verify that a sufficient, minimum level of details and detailing is included on each set of structural drawings and shop drawings. Minimum level of detailing to comply with requirements of ACI publications as noted in current NYC Building Code.* 

Current Department of Buildings plan review procedures do not include technical review of constructability; therefore, design drawings submitted by design professionals often lack consideration of overall constructability. Including a sufficient level of proper detailing on structural drawings will minimize onsite confusion, increase construction efficiency, and reduce potential structural defects and inadequacies resulting from designed-in bar congestion (Figure B.10.1- B.10.3).

A monitoring program supervised by a qualified engineer familiar with practical construction sequencing considerations is warranted based on practices in major municipalities. Optimally, this professional would have experience as a constructability analyst for a general contractor, in addition to considerable design experience. Similar to the structural quality review recommendation, the city should maintain in-house staff sufficient to audit a percentage of completed constructability reviews.



**Figure B.10.1: Splice Condition Requiring Additional Information from the Engineer of Record.** 



**Figure B.10.2: Constructability Issues at Beam-Column Connection** 



**Figure B.10.3: Constructability Issues at Transfer Beam top bars** 

**Appendix B.1: Site Observation Log** 




















































**Appendix B.2: Comparative Concrete Testing** 

A preliminary audit of concrete property reporting was performed by the HRCO. Comparisons were made between results provided by the labs in question with results provided by an independent laboratory (The Port Authority of New York and New Jersey). The following assessments of five labs (designated A through E) were made by HRCO staff, and included some facilities visited during the Laboratory Quality assessment.

TESTING LAB: A

SITES: Site 87, 15-October 2008

Site 72, 12-November 2008

The following report provides comments regarding the sites sampled by the HRCO and Test Well on the date and site noted above.

#### **Testing Methods**

In accordance with ASTM C94 "Standard Specification for Ready-Mixed Concrete" concrete should be tested for unit weight and air content in conformance with ASTM C138 "Standard Test Method for Density (Unit Weight), Yield, and Air Content (Gravimetric) of Concrete" and ASTM C231 "Standard Test Method for Air Content of Freshly Mixed Concrete by the Pressure Method" respectively.

During the field sampling performed by this lab, it was observed that neither ASTM compliant unit weight testing, nor any surrogate unit weight test method was performed. Air testing was performed using the chase air indicator which is not an ASTM standard, and as noted by the manufacturer of the product, does not qualify as a substitute for the pressure or volumetric method prescribed by ASTM. Test reports do not indicate the test methods by which air content and unit weight were obtained, although the report suggests full ASTM conformance by making reference to ASTM C94.

### **Reporting Of Test Results**

Compressive strength test results, as prescribed by ASTM C39 "Standard Test Method for Compressive Strength of Cylindrical Concrete Specimens", should be reported at the age of 24 hours, 3 days, 7 days, 28 days, and 90 days within their respective tolerances unless otherwise required in the project specifications. Compressive strength test results of individual cylinders reported for both sites do not comply with the age requirements set forth in ASTM C39. In the case of Site 87, samples prepared on 15-Oct. 2008, were tested at an age of 37 days, and no testing was performed at 28 days. The Site 72 samples prepared on 12-Nov. 2008 were tested at 10 days, 29 days and 37 days. There is a possibility that the 29 day test result is within

tolerance, although the time of day at which the samples were prepared and tested is not provided.

Lab test reports indicate fracture pattern type 5. This fracture pattern is typically found in tests performed with un-bonded caps. When this type of fracture occurs during testing, ASTM C39 recommends continuing compressing the specimen until a different fracture is achieved. Therefore, these results further suggest this lab's non-conformance with ASTM standards.

### **Test Results**

The following table presents the test results for the sites sampled by the HRCO and Lab A. Test results were extracted from reports provided by the Department of Buildings' independent laboratory, The Port Authority of New York and New Jersey.

<b>Site</b> Location (date)	<b>Testing</b> <b>Agency</b>	ID	Air (%)	<b>UW</b> (Ibs/cuft)	<b>Specified</b> strength (psi)	Age (days)	Average f'c (psi)	% based on 28 day strength
	Port Authority	Site 87	1.6	152.8		$\,6$	7450	70
						$\overline{28}$	10665	100
						$\overline{7}$	7630	<b>NA</b>
		set 3 set 5	2.2 2.0	152		$\overline{37}$	11060	<b>NA</b>
Site 87						56	11105	<b>NA</b>
(10/15/2008)				151	9000	$\overline{7}$	8270	<b>NA</b>
	Lab A					37	11940	<b>NA</b>
						56	11990	<b>NA</b>
			2.2	152		$\overline{7}$	8370	<b>NA</b>
		set 8				37	11460	$\sf NA$
						56	12190	<b>NA</b>

**Table 1. Summary of Concrete Compressive Strength Results at Site 87** 

<b>Site</b> Location (date)	<b>Testing</b> Agency	ID	Air $(\%)$	<b>UW</b> (Ibs/cuft)	<b>Specified</b> strength (psi)	Age (days)	Average f'c (psi)	% based on 28 day strength
Site 72 (10/27/2008)	Port Authority	Site 72	$\overline{5}$	148.8		$\overline{7}$ 28	4800 6370	75 100
	Lab A set 1	3	149	5000	10 29	4850 5280	<b>NA</b> 100	
						37	5440	<b>NA</b>

**Table 2. Summary of Concrete Compressive Strength Results at Site 72** 

General Comments:

- Strength development rends are typical
- The Site 87 strength test results for specimens at 6 and 7 days, are similar for both testing agencies.
- At Site 72, strength development rate of the concrete specimens appears lower than those sampled by HRCO engineers. The rate at which concrete develops strength is related to the mix proportions, curing time and curing temperature.

TESTING LAB: B

SITES: Site 56, 21-October 2008

Site 41, 23-October 2008

Site 14, 5-November 2008

The following report provides comments regarding the sites sampled by the HRCO and Laboratory B on the date and site noted above.

### **Testing Methods**

In accordance with ASTM C94 "Standard Specification for Ready-Mixed Concrete" concrete should be tested for unit weight and air content in conformance with ASTM C138 "Standard Test Method for Density (Unit Weight), Yield, and Air Content (Gravimetric) of Concrete" and ASTM C231 "Standard Test Method for Air Content of Freshly Mixed Concrete by the Pressure Method" respectively.

 HRCO engineers were present at three sites where this lab generated an "Inspection and Testing of Concrete Report" which summarized information related to the concrete placement on a specific date and the strength of the corresponding specimens. HRCO engineers observed test methods utilized by this lab during their sampling of fresh concrete properties, and observed they failed to perform unit weight testing. Furthermore, air content testing was performed using the chase air indicator, which is not an ASTM standard and, does not qualify as a substitute for the pressure or volumetric method prescribed by ASTM.

Lab test reports produced by lab B do not indicate the test methods by which air content and unit weight were obtained, or if test methods were performed in accordance to the standards recommended by ASTM C94.

### **Reporting Of Test Results**

Compressive strength test results should be reported in accordance with ASTM C 39 "Standard Test Method for Compressive Strength of Cylindrical Concrete Specimens". The standard indicates that the fracture pattern produced by compressive testing should be included in the test report. The reports produced by this lab indicate the fracture pattern for *all* cylinders, even those not subjected to compressive testing, is type "A", suggesting this classification is a "default" pattern on the spreadsheet used to generate the report. Reporting in this manner raises concerns regarding the accuracy of lab B's test reporting.

### **Test Results**

The following table presents the test results for the sites sampled by HRCO engineers and Lab B. Test results were extracted from reports provided by the Department of Buildings' independent laboratory, The Port Authority of New York and New Jersey.



### **Table 1. Summary of Concrete Compressive Strength Results at Site 56**

<b>Site</b> Location (date)	<b>Testing</b> <b>Agency</b>	ID	air (%)	<b>UW</b> (lbs/cu ft)	<b>Specified</b> strength (psi)	Age (days)	f'c(psi)	% based on 28 day strength
	Port Authority		1.5	150		$\overline{7}$	4570	74
						28	6176	100
	Lab B	1S	3.0	153		$\overline{7}$	4980	80
Site 41					5000	29	6250	100
(10/23/2008)		2S	2.4	155		$\overline{7}$	4790	79
						28	6043	100
		3	2.7	153		$\overline{7}$	4920	76
						28	6453	100

**Table 2. Summary of Concrete Compressive Strength Results at Site 41** 

<b>Site</b> Location (date)	<b>Testing</b> <b>Agency</b>	ID	air (%)	<b>UW</b> (lbs/cuft)	<b>Specified</b> strength (psi)	Age (days)	f'c(psi)	% based on 28 day strength
	Port					$\overline{2}$	6510	<b>NA</b>
	Authority		3.3	152		$\overline{7}$	8420	<b>NA</b>
						28		<b>NA</b>
Site 14	Lab B	<b>10S</b>				$\overline{7}$	9690	81
(11/5/2008)			1.9	150	8000	14	10780	91
						28	11910	100
				153		$\overline{7}$	8580	$\overline{75}$
		<b>11S</b>	1.5			14	9830	86
						28	11400	100

**Table 3. Summary of Concrete Compressive Strength Results at Site 14** 

General Comments:

• Trends in strength development and strength levels are similar for both testing agencies

### TESTING LAB: C

SITE: Site 16, Manhattan 29-October, 2008.

The following report provides comments regarding the sites sampled by the HRCO and Laboratory C on the date noted above.

#### **Testing Methods**

In accordance with ASTM C94 "Standard Specification for Ready-Mixed Concrete" concrete should be tested in for unit weight and air in conformance to ASTM 138 "Standard Test Method for Density (Unit Weight), Yield, and Air Content (Gravimetric) of Concrete" and ASTM 231 "Standard Test Method for Air Content of Freshly Mixed Concrete by the Pressure Method" respectively.

During the field sampling performed by HRCO engineers at Site 16, it was observed that laboratory staff did not perform ASTM compliant unit weight or air content testing. Test reports do not indicate the test methods by which air content and unit weight were obtained and reported.

#### **Reporting of Test Results**

Compressive strength test results should be reported in accordance with ASTM C 39 "Standard Test Method for Compressive Strength of Cylindrical Concrete Specimens". Strength test results reported by this lab do not list the type of fracture pattern as prescribed by ASTM C39. This particular item is of importance because cylinders tested with unbonded caps are likely to exhibit varying fracture patterns, and an analysis of these patterns by the engineer may indicate if the cylinder's ultimate strength has been appropriately reported.

ASTM C39 also requires that specimen size, loaded area of cylinder, and load levels be reported on standard laboratory reports. Test reports provided by lab C failed to provide this information.

#### **Test Results**

The following table presents the test results for the site sampled by HRCO engineers and Laboratory C. Test results were extracted from reports provided by the Department of Buildings' independent laboratory, The Port Authority of New York and New Jersey.

<b>Site</b> Location (date)	<b>Testing</b> <b>Agency</b>	<b>Field</b> ID	Lab ID	air $(\%)$	<b>UW</b> (lbs/cuft)	Age (days)	f'c (psi)	$\%$ based on 28 day strength
	Port					2	3170	58
	Authority			8.0	140	$\overline{7}$	3810	70
						28	5435	100
Site 16		175	1819- 1822	4.0	141	$\overline{7}$	3970	75
(10/29/2008)						28	5260	100
	Lab <sub>C</sub>	178	1830- 1833	4.5	145	$\overline{7}$	4490	69
						28	6490	100
		180	1838- 1840	4.5	144	28	6010	100

**Table 1. Summary of Concrete Compressive Strength Results at Site 16** 

General comments:

• Trends of the concrete strength development appear similar for testing performed by both laboratories

### TESTING LAB: D

SITES: Site 67, 10-October 2008

Site 4, 15-October 2008

Site 79, 12-November 2008

The following report provides comments regarding laboratory D test sites observed by the HRCO on the dates noted above.

### **Testing Methods**

Reports prepared by Lab D indicate that unit weight and air content testing should be performed in accordance to ASTM C138 "Standard Test Method for Density (Unit Weight), Yield, and Air Content (Gravimetric) of Concrete", and ASTM C231 "Standard Test Method for Air Content of Freshly Mixed Concrete by the Pressure Method" respectively. During the field sampling performed by HRCO engineers at these sites, it was observed that Lab D did not perform any ASTM-compliant unit weight testing. Furthermore, air content testing was performed using the chase air indicator, which is not an ASTM standard, and does not qualify as a substitute for the pressure or volumetric method prescribed by ASTM.

### **Reporting Of Test Results**

Compressive strength test results, including fracture pattern, must be reported in accordance with ASTM C39 "Standard Test Method for Compressive Strength of Cylindrical Concrete Specimens". Strength test results reported by this laboratory do not list the type of fracture pattern as prescribed by ASTM C39. This particular item is of importance because cylinders tested with un-bonded caps are likely to exhibit varying fracture patterns, and an analysis of these patterns by the engineer may indicate if the cylinder's ultimate strength has been appropriately reported.

### **Test Results**

The following table presents the test results for the sites sampled by HRCO engineers and laboratory D. Test results were extracted from reports provided by the Department of Buildings' independent laboratory, The Port Authority of New York and New Jersey

<b>Site</b> Location (date)	<b>Testing</b> <b>Agency</b>	<b>Specified</b> strength (psi)	ID	Air $(\%)$	Unit Weight (Ibs/cuft)	Age (days)	Average f'c (psi)	Percentage of 28 day f'c
						$\overline{2}$	4350	42
	Port Authority		Site 67	2.8	149.6	$\overline{7}$	7395	72
						28	10325	100
	Lab D	7000	3250E	2.5	149.9	$\overline{7}$	8490	82
Site 67 (10/10/2008)						28	10417	100
			3250B	2.25	149.9	$\overline{7}$	8435	86
						28	9830	100
			3250G	2.0	149.9	$\overline{7}$	7980	85
						28	9440	100

**Table 1. Summary of Compressive Strength Test Results at Site 67**

<b>Site</b> Location (date)	<b>Testing</b> <b>Agency</b>	<b>Specified</b> strength (psi)	ID	Air (%)	Unit Weight (Ibs/cuft)	Age (days)	Averag e f'c (psi)	Percentage of 28 day f'c
	Port Authority		Site 4	1.6	149.6	6	8630	67
						28	12970	100
		8300	3304A	2.0	149.9	$\overline{7}$	6360	73
Site 4 (10/15/2008)	Lab D					28	8703	100
			3304B	2.25	149.9	$\overline{7}$	6480	75
						28	8640	100
			3304C	2.5	149.9	$\overline{7}$	6230	75
						28	8340	100

**Table 2. Summary of Compressive Strength Test Results at Site 4** 

### **Table 3. Summary of Compressive Strength Test Results at Site 79**



• Port Authority and laboratory D strength test results exhibit similar trends and strength development

- Average compressive strength results provided by this lab, corresponding to sites 79 and 4, were consistently lower than those tested by the Port Authority. The approximate difference in average strength at 28 days was 35%.
- Strength levels, based on a percentage of the 28 day strength, were generally 10% lower for the results reported by lab D when compared to the data provided by the Port Authority.

### TESTING LAB: E

SITE: Site 85, 23-October 2008

The following report provides comments regarding the sites visited by the HRCO and Laboratory E on the dates noted above. HRCO did not sample concrete from this site, but specimens from which strength results were obtained were provided to the HRCO by lab E and the Department of Buildings' independent laboratory, The Port Authority of New York and New Jersey.

### **Testing Methods**

ASTM C94 "Standard Specification for Ready-Mixed Concrete" dictates proper test procedures for concrete testing. According to ASTM C94, unit weight and air content testing should be performed in conformance to ASTM C138 "Standard Test Method for Density (Unit Weight), Yield, and Air Content (Gravimetric) of Concrete" and ASTM C231 "Standard Test Method for Air Content of Freshly Mixed Concrete by the Pressure Method" respectively. At this site, lab E did not perform any ASTM-compliant unit weight testing. Furthermore, air content testing was performed using the chase air indicator, which is not an ASTM standard, and does not qualify as a substitute for the pressure or volumetric method prescribed by ASTM.

Lab test reports produced by this lab do not indicate the tests methods by which air content and unit weight were obtained, or if test methods were performed in accordance to the standards recommended by ASTM C94.

### **Reporting Of Test Results**

Compressive strength test results should be reported in accordance with ASTM C 39 "Standard Test Method for Compressive Strength of Cylindrical Concrete Specimens". Strength test results reported by ASC do not list the type of fracture pattern as prescribed by ASTM C39. This particular item is of importance because the analysis of the fracture pattern by the engineer may indicate if the cylinder's ultimate strength has been appropriately reported.

### **Comparison of Test Results**

Laboratory E reported on 23-October 2008, that twenty-five (25) 4"x8" cylinders were set aside for the HRCO including fourteen (14) cylinders specified at 7000 psi, and eleven (11) cylinders specified at 9000 psi.

Upon returning to the site, the HRCO found only three of the reported eleven 4"x8" 9000 psi cylinders. Table 1 compares the results of concrete testing as reported by lab E and the HRCO's independent laboratory. The compressive strength results provided by this lab are not consistent with cylinder dimensions reported in the field. Data suggests lab E either failed to accurately field-report cylinder dimensions, or fabricated compressive strength data for nonexistent cylinders. It is unknown if lab E possesses the equipment necessary to load a specimen to 360 kips.



#### **Table 1. Reported Cylinder Properties**

**\*Data obtained from laboratory report dated 23-October 2008-Specimen 81G** 

**\*\*Cylinder size contrary to that documented in field report** 

#### **Test Results**

The following table presents the test results for the sites sampled by lab E, and provided to the HRCO. Test results were extracted from reports provided to the Department of Buildings.

<b>Site</b> Location (date)	<b>Testing</b> <b>Agency</b>	ID	air (%)	<b>UW</b> (Ibs/cuft)	<b>Specified</b> strength (psi)	Age (days)	f'c (psi)	% based on 28 f'c
	Port Authority	N/A	N/A	N/A		$\overline{7}$	6330	80
						$\overline{28}$	7885	100
		79	5.0	147	7000 psi	$\mathbf{1}$	3890	
	Lab E					$\overline{7}$	6760	
		80	5.5	147		1	4320	
						$\overline{7}$	6530	
Site 85	Port Authority	N/A	N/A	N/A		$\overline{7}$	9410	$\overline{78}$
(10/23/2008)						28	12070	100
				153	9000 psi	$\mathbf{1}$	4780	38
		81	2.0			$\overline{7}$	10390	82
	Lab E					28	12637	100
				153		$\overline{1}$	4780	41
		82	1.0			$\overline{7}$	10100	86
						28	11745	100

**Table 2. Summary of Concrete Compressive Strength at Site 85** 

General Comments:

• Compressive strength development and results appear similar for both testing agencies.

**Appendix B.3: Laboratory Quality Observations** 

After assessing the testing procedures and results from a number of concrete testing laboratories, the HRCO team concluded that laboratory quality varies greatly and that continued monitoring of the laboratory's ability to perform ASTM-compliant testing is well warranted. The following observations of three labs (designated D, E, and F) were made by HRCO staff in January 2008.

#### **Testing Lab D**

The following observations were compiled during an HRCO team visit to Testing Laboratory D conducted on January 22, 2008:

- Lab employs at least three ACI certified strength testing technicians
- Observed organized curing room and laboratory record-keeping.
- Lab utilizes automated testing equipment for application of load.
- Insufficient record keeping in regards to reusable neoprene caps.
- Test results fail to record compression failure mode. Lack of notation not in conformance with ASTM C31.

#### **Testing Lab E**

The following observations were compiled during an HRCO team visit to Testing Laboratory E conducted on January 22, 2008:

- Cylinder de-molding occurred four days after delivery, timing not in conformance with specifications of ASTM C31.
- Cylinders only partially immersed in water, not in conformance with specifications of ASTM C31 (Figure B.3.1).
- Lack of proper water circulation in curing trough. Temperature of water in trough is 10° higher than allowed by ASTM C31.
- Lack of certified personnel (ACI strength testing technician)
- Compression equipment not automated, technician must indirectly control loading rate.
- Lack of humidity sensor in curing room.
- Insufficient equipment available to properly measure core or cylinder dimensions.
- Final reports lack reference to testing methods or ASTM standards.

• Test results fail to record compression failure mode. Lack of notation not in conformance with ASTM C31.



#### **Figure 1: Improper Cylinder Curing Procedures, Some Cylinders Partially Immersed**

#### **Testing Lab F**

The following observations were compiled during an HRCO team visit to Testing Laboratory F conducted on January 21, 2008:

- No ACI certified strength testing technicians present during visit.
- Curing room appeared to contain adequate temperature and moisture conditions and controls.
- Cylinder storage not organized, cylinders stacked on top of each other.
- Records indicate that testing machines were recently calibrated, however, the loading system is not automated, and the rate of loading must be controlled manually.
- Unbonded neoprene cap records indicate some caps were used more than One hundred times, exceeding provisions of ASTM C1231 / C1231M – 09: *Standard Practice for Use of Un-bonded Caps in Determination of Compressive Strength of Hardened Concrete Cylinders*.

Test results fail to record compression failure mode. Lack of notation not in conformance with ASTM C31.
# **C. Cranes and Hoists**

# **C.1 INTRODUCTION**

This chapter summarizes the crane and hoist assessment, and includes this introduction (Section 1), aspects of crane safety (Section 2), observations completed during assessment period (Sections 3), DOB process review and industry outreach (Section 4) and a summary of the recommendations (Section 5). Crane Tech Solutions and Patuxent Engineering Group principally authored the crane and hoist sections of this chapter, respectively.

The overriding themes of these recommendations are the importance of knowledgeable and experienced workers (both industry and regulatory), promotion of oversight and modernization of equipment.

From all sources available to the HRCO: historical studies; meetings with industry, manufacturers and DOB; and, our own experience, the most important factor for safe crane operations is having knowledgeable and experienced workforce. Recommendations for crane erection, climbing and disassembly, third party inspections, maintenance & repair all serve to increase the level of knowledge and experience available to the crane workforce during critical operations.

Promotion of oversight seeks to make DOB more efficient in its role. Recommendations such as Tracking Mobile Cranes (to improve the ability of DOB to observe these machines), Third Party Inspections (which remove the day-to-day resource obligations for inspections from DOB) and Maintenance & Repair (which allows tracking of critical crane repairs) all streamline DOB's ability to enforce regulations. Many of the issues identified by the HRCO are already addressed by existing regulations; what is needed is the ability to efficiently enforce the regulations and identify the minority of individuals and companies that are habitually out of conformance.

Modernization of equipment will provide many benefits. In general the recommendations do not specifically call for changes in equipment, but many of the issues addressed by the recommendations would be improved with a newer fleet. For example, a number of marginal rigging practices, such as those associated with "riding a load" (in which a worker must stand on a piece of equipment while it is being lifted), would be obviated by employing newer tower cranes.

These themes are reflected in recommendations regarding Crane & Derricks Unit (C&D) operations, and in many ways have already been taken up by C&D following a recent restructuring. For example, C&D is working to enhance staff training in many ways including additional hands-on training for field inspectors and exposing plan examiners to field inspections. Also, C&D has been working to improve and streamline

its approach to oversight with initiatives such as formalizing Standard Operating Procedures and development of a database that will ultimately be accessible by the public.

In additional to assessing crane operations, the HRCO team identified a gap in regulation of hoist equipment in NYC. There is potential for significant accidents and injuries associated with these machines. Therefore the HRCO included assessments of hoist machines as a subset of the crane study.

# **C.2 Aspects of Crane Safety**

## Accident Causes

Crane safety is an important component of overall construction safety. The Occupational Safety and Health Administration (OSHA) compiles national data on both general construction and crane-specific accidents. Studies of the OSHA data identify crane accidents to be associated with  $8\%^1$  to 16.1%<sup>2</sup> of construction fatalities.

The variation is not surprising; as important as crane operations are, the available national crane accident data is far from complete. In the first place, many crane accidents go unreported. For those that are investigated by a regulatory authority, there is no consistent, master database of crane accident records across the country. For the most part, studies of historical data require in-depth review of actual accident reports to identify causal factors. Numerous studies of OSHA data have endeavored to identify leading factors that cause accidents, some of the most notable lists of accident causes are summarized in Table C.1.1.

Center to Protect Worker's Rights $(CPWR)^3$		Sheppard et. al. (2000) <sup>4</sup>		Construction Industry Research and Policy Center (CIRPC) <sup>1</sup>	
Source: Selected OSHA records for 1984 - 1994		Source: Selected OSHA records for 1984 - 1994		Source: OSHA Records for 1997- 2003	
Cause	Percent	Cause	Percent	Cause	Percent
Electrocution	39%	Electrocution	36%	Struck by load	32%
Assembly/Dismantling	12%	Fall of load	10%	Electrocution	27%
Boom Buckling	8%	Overturn	7%	Assembly/disassembly	12%
Upset/overturn	7%	Dismantling	6%	Failure of boom/cable	12%
Rigging	7%	Caught b/n counterweight	3%	Tip over	11%
Other	27%	Other	38%	Struck by cab/counterweight	3%
				Falls	2%

**Table C.1.1: Summary of Crane Accident Study Findings** 

<sup>1</sup> Beavers, J.E. et.al., Crane-Related Fatalities in the Construction Industry, *University of Tennessee Construction Industry Research and Policy Center (CIRPC)*, March, 2005.

<sup>2</sup> Neitzel, R.L., et.al., A Review of Crane Safety in The Construction Industry, *Applied Occupational and Environmental Hygiene* 16(12), 2001.

 $3$  McCann, M., et.al., Crane-Related Deaths in Construction and Recommendations for Their Prevention, The Center for Construction Research and Training (CPWR).

<sup>4</sup> Shepard, G.W., et.al., Crane Fatalities – A Taxonomic Analysis, *Safety Science* 36(2), 2000.

Similarly, a 2009 study from the Technion-Israel Institute of Technology is a first step in an attempt to determine, with greater accuracy, factors that influence crane safety. This first phase of the study involved a detailed survey of crane experts. Twenty one primary factors that effect crane safety were identified and weighted.



**Figure C.1.1: Weighting of Factors that Affect Crane Safety.** 

These factors have varying degrees of relevance to the New York crane environment. The most significant point being that the study of causes of crane accidents is still in its infancy and that there are a wide range of factors that cause accidents. There is only a general understanding of leading causes, and little clear guidance on factors and practices that would best reduce accidents. Perhaps the most common theme is the role of human error in a majority of accidents and the related importance of worker knowledge and experience to avoid failures.

## Consequence and Impact

What will be termed *high-consequence* crane accidents are of particular concern for the HRCO study. High-consequence crane accidents are generally associated with tower and large mobile cranes, and are qualitatively differentiated as having a high potential for multiple fatalities (including bystanders) and significant destruction of property.

Based on HRCO analysis of historic NYC accident data, between January 2006 and December 2008, 75% of fatalities and 55% of injuries were associated with just three

major tower crane failures (Table C.1.2). One failure in particular (March 15, 2009 51<sup>st</sup> failure) accounted for 58% and 42% of fatalities and injuries, respectively.



**Table C.1.2: NYC Crane injuries and fatalities for three year period, January 2006 – December 2008.** 

The high-consequence of accidents involving tower and large mobile cranes is a function of the size of the machines and magnitude of load that they are capable of lifting. Typical tower and large mobile cranes have impact diameters of hundreds of feet (based on the height and reach of the cranes). The equipment itself typically weighs tens of thousands of pounds and is capable of lifting hundreds of thousands of pounds.

Figure C.1.2 shows an impact zone with a 200 foot radius. Within this zone are dozens of buildings and on the order of 1,000 people. The hypothetical impact zone is shown for an actual past crane location, and one at which there was a significant failure during dismantling of the crane.

As is the nature of most high-consequence events, the probability of major crane accidents is low. Along with low probability of occurrence, there is also a low probability of repetition of cause. The HRCO is not aware of any authoritative set of data of high-consequence crane failures. An informal list compiled by the HRCO identified that after assembly, climbing and dismantling; there was little repeatability in the source of the accidents.



**Figure C.1.2: Impact Zone of a Tower Crane Collapse.** 

The combination of low probability and high variability (and thus uncertainty) of causes of high-consequence crane accidents presents a challenge in promoting safety. Construction risks which are closely tied to a single cause can be addressed by targeted procedures. The variable nature of crane risk requires a broader range of controls to introduce a level of redundancy.

# **C.3 Site Observations**

## Cranes

A total of 182 site visits were completed by HRCO crane field teams between July 2008 and January 2009. Of these, there was no crane or no observable crane operations at 14 sites, resulting in 168 actual observations of crane equipment and operations, carried out on 104 individual pieces of equipment (some cranes were observed multiple times). Table C.3.1 provides the type and number of the various types of cranes visited.

The crane team typically sent out one senior inspector to visit each site. The team performed full and targeted visits. Targeted site visits were limited to specific crane safety issues. Full site visits included a broad spectrum of items related to crane equipment and operation. A DOB Cranes and Derricks Unit inspector accompanied the HRCO observation teams during a substantial number of the early site visits. The HRCO completed the later visits alone and reported any potential violating conditions directly to C&D. Observations from site visits were recorded on to standardized *Location Reports*.

The HRCO team essentially observed all available tower crane sites during the period of the study. There may have been a small number of tower cranes that were either being just brought out of or into operation at beginning or end of the study that were not observed.



## **Table C.3.1 – Types of cranes visited**

The majority of mobile cranes were observed in September and October 2008. Forty jobsites were chosen randomly from the outstanding list of permitted cranes. Jobsites in the Bronx, Brooklyn, Manhattan and Queens where selected. Additional mobile crane observations were made based on particular issues of interest.

## **Hoists**

A total of 99 site visits were completed by the HRCO hoist team between July 2008 and January 2009. Because of the relatively little oversight currently applied to hoist machines, hoist sites were selected on a random basis and captured a range of parameters including type (material only and personnel and material hoists), union and non-union operation and configuration of back structure.

Nine of the hoist site observations were targeted to hoist machine owner's shops and storage yards as described in the recommendation for Off-site Controls.

# **C.4 DOB Process Review and Industry Outreach**

## DOB Process Review

The HRCO team interviewed all of the Cranes and Derricks Unit's inspectors (through February, 2009) to determine their respective strengths and weaknesses as well as to determine their views regarding the unit and industry. The HRCO crane team also observed inspectors in the field performing their inspection tasks.

In addition to the inspectors, the HRCO crane team interviewed the plan examiners and members of the administrative staff. The purpose of these interviews was to assess the various procedures of the Unit and the functioning of the staff.

### Industry Outreach

An important aspect of the overall assessment was to include the various perspectives of the stakeholders in the crane area. To do this, the HRCO moderated three meetings with the NYC industry. The attendees included: crane owners, users, professional engineers, manufactures, union representatives, operators and DOB personnel. The HRCO presented their proposed recommendation and sought feedback from the group. These meeting were valuable in shaping the final recommendations.

DOB and the HRCO also wanted to include other groups that may have a viewpoint for the recommendations. As such, DOB moderated a meeting with other regulatory bodies to share ideas and determine possible directions for the jurisdiction. In addition, the HRCO moderated two meetings with manufacturers to outline the possible recommendations. These groups were also critical in the final development of this report.

There were three new laws enacted in the fall of 2008 to primarily tower cranes. One of these laws required the members of tower crane crews (assembly, jumping and dismantling) to attend a 30 hour course. The HRCO attend a four hour portion of one course to ascertain the curriculum and the class room environment. In addition, the material for two other courses was reviewed for content.

New York State invited the HRCO to attend one of their practical test sites to observe its hoist machine operator test. This was held in Long Island in December. In addition, the HRCO viewed the practical test for the NCCCO on their web site.

## **C.5 Summary of Recommendations**

Recommendations fall into subcategories: Equipment Design, Site Specific Design, Crane Operations, Inspection, Maintenance and Repair and DOB Internal Operations. These categories essentially cover the entire life cycle of a crane, from creation (design and manufacture) through retirement. Recommendations that are specific to hoist equipment come at the end of each category.

Recommendations designated as *Further Study* are those that may require additional investigation on the part of DOB to fully gauge their applicability or usefulness. Recommendations are summarized as follows:

## **Equipment Design**

## **Approved Manufacturer (C-7)**

 Replace the current model-specific Certificate of Approval process with one that approves the manufacturer using predetermined, industry-standard criteria.

### **Older Equipment (C-14) (Further Study)**

 Require an extensive mechanical crane inspection every 10 years for all cranes and potentially an age limitation for operation in the jurisdiction.

### **Electric Tower Cranes (C-21) (Further Study)**

Have an all-electric tower crane fleet in the jurisdiction by a specified date.

### **Hoist – Equipment Acceptance (H-1) (Further Study)**

Create and implement an Equipment Acceptance Certification program for hoisting equipment employed in the NYC area.

### **Site Specific Design**

### **Tie-Ins (C-8)**

Tie-In connections should be subjected to special inspection and require improved design and erection procedures

### **Foundations (C-9)**

 Foundations should be subjected to special inspection and require improved design and erection procedures

### **Load Test (C-15)**

 The test weights to be used should not exceed the manufacturer's specification or, in case where the manufacturer is not available, the applicable ANSI standard should be followed.

## **Counter Weights (C-5)**

 Counter weight information should be readily available on the drawing and on the counter weight module itself.

## **Hoist – PE Sign-off (H-2)**

Require the building engineer of record or an engineer acceptable to DOB to review that the building can support the loads imposed by the hoist.

## **Crane Operations**

## **Rigging Safety (C-4)**

Establish a DOB sanction group to review current industry practices, how they differ from the regulations, and determine the best means to enforce current regulations. The practice of dragging or side pulling the load should be eliminated. The 30 hour tower crane rigger class should devote a substantial portion of its curriculum on the erection, climbing and dismantling of tower cranes as well as general rigging.

## **Articulating Boom Crane (C-12)**

 The definition of "crane" should be changed so that articulating boom cranes are regarded as a special type of crane. This, in turn, would require each such crane to have an annual inspection (Certificate of Operation) and a licensed operator (HMO).

## **Crane Assembly (C-13)**

 All assembly, climbing and dismantling of a tower crane must include the on-site participation of a Technical Advisor who is one of the following:

- 1. A representative from the Original Equipment Manufacturer (OEM)
- 2. A qualified, factory trained representative of the distributor / OEM
- 3. A qualified, factory trained owner's representative

## **HMO "C" License (C-1)**

Require National Crane Operator Certification for Hoisting Machine Operator "C" License Examination.

## **HMO "A" and "B" License (C-23)**

Require all Hoist Machine Operators (HMOs) to have a nationally recognized certificate and ensure each operator has the necessary experience to operate the cranes they use.

## **Scaffolding Hoist (C24) (Further Study)**

DOB should require a plan review and inspection of custom built hoisting systems that are able to hoist loads exceeding 1 ton (907 kg).

## **Hoist – Riding on Top of Cars (H-3) (Further Study)**

Restrict actions of workers riding on top of cars to limit inherent dangers of working on and in close proximity to moving equipment.

### **Inspection**

## **Third Party Inspection (C-3)**

 Allow third party inspectors (inspectors from entities independent from DOB and the crane owner or user) to perform the required annual crane inspections needed for the CD permit.

### **Bolted Connections (C-2)**

 All bolted connection must be checked regularly. Crane maintenance personnel must have basic knowledge about bolt torquing (see C-R-06).

### **Tracking Mobile Cranes (C-17)**

 Require the crane user/owner of mobile cranes to notify DOB prior to the start of a job and when the crane will leave the jobsite. DOB must also be notified if there are changes in the schedule. The notification is required for all jobs that require a Certificate of onsite inspection.

### **Hoist – ANSI Standards (H-4)**

 Adopt the ANSI A10.5 Material Hoist standard. Regularly update regulation to reflect current versions of A10.5 (Material Hoist) and A10.4 (Personnel and Material Hoist).

### **Hoist – Qualified Inspections (H-5)**

 Introduce a "Qualified Hoist Inspection" Program that establishes the requirements and qualifications of the inspectors performing inspections of temporary personnel and material hoists inspections, as well as the inspection criteria and Drop Test Reports that are filed with DOB after the inspections are performed.

### **Maintenance and Repair**

### **Maintenance and Repair (C-6)**

Repair: The Owner must notify DOB of all major structural repairs while the component is actively registered (has CD) or upon renewal if the CD lapsed

 Maintenance: Increase the written maintenance and inspection log requirements to provide more complete records of the work performed on each crane.

### **Component Tracking (C-20)**

DOB should institute a tracking system for the major structural components

### **Data Recorder – "Black Box" (C-22) (Further Study)**

 Based upon further study, DOB should consider the use of data recording devices that will provide critical information regarding the operation of cranes within the jurisdiction.

## **Hoist – Off-site Controls (H-6) (Further Study)**

 Introduce and implement an Off-site Hoist Equipment Control Program to check that the equipment is adequate for the intended use.

## **Hoist – On-Site Log Book (H-7)**

 Require that all site locations maintain an On-Site Hoist Equipment Log to standardize record keeping of all pertinent data.

## **DOB Operations**

## **Inspector and Examiner Training (C-11)**

 Assess the various skill sets of the inspectors and plan examiners of the Department of Buildings and provide them the necessary training and tools to complete their tasks effectively and efficiently

## **Accident Investigation (C-18)**

 The Crane and Derrick Unit should augment and audit its incident/accident reporting procedure to confirm each file contains the required information and the inspectors' investigation is organized and thorough.

## **C&D Self Auditing (C-19)**

 Develop and install a change process whereby the Cranes and Derricks Unit of the Department of Buildings monitors itself and makes adjustments as necessary

## **RS 19.2 (C-16)**

DOB should revise of RS 19-2 and seek industry comments.

## **Hoist – Regulation of Hoists (H-8) (Further Study)**

 Hoist equipment (Personnel and Material Hoists and Back-Structures) should be subjected to engineering review, permitting and site inspection by a dedicated DOB department.

## **C.6.2 Recommendation C-7: Approved Manufacturer**

*Replace the current model-specific Certificate of Approval process with one that approves the manufacturer using predetermined, industry-standard criteria.*

## **C.6.2.1 Description**

The City of New York approves each crane model prior to its operation within the jurisdiction (proto type approval). The basic tenet of this regulation comes from the need to ensure that the cranes operating within the jurisdiction comply and were designed based upon applicable standards and the Department of Buildings having the necessary information to inspect and audit the cranes installation and activities. To shorten the prototype approval process, this recommendation will describe a means to institute an alternative whereby manufacturers are approved versus individual cranes.

To obtain the "approved" status, the manufacturer would have to meet a set of criteria such as: willingness to add the Department of Building onto their safety recall notice list, adhere to a list of standards used in designing and manufacturing cranes, keep DOB informed if substantial changes are made to the cranes, have a commitment to the area to address repair procedures (can be accomplished with a dealer network however the dealer should have technicians trained by the OEM), provide electronic manuals, and possibly others.

The "Approved" manufacturer is common in the internal purchasing procedures of public and private organizations. This method is typically used to shorten the procurement cycle and to use companies that have met specific criteria. For instance, the State of Texas issues a list of preferred manufacturers for school buses, which in turn, are procured by the individual school boards.



## **C.6.2.2 Recommendation Approach**

Persons currently submitting a Certificate of Approval "Prototype Crane Application" can be crane owners, crane rental agencies, crane distributors or any other groups interested to operate a crane. A change of configuration of an already- approved crane (such as adding tower heights, boom or jib length or other major modifications) requires only additional documentation on the specific change to be resubmitted for a new certificate of approval.

Under the current system, an Engineer of Record (EOR) submits the application with the information outlined in DOB's Reference Standard 19-2. This information consists of information supplied primarily by the manufacturer, such as operating manuals, calculations on the design, the material used and the standards used to design the crane, among others.

DOB then reviews the submittal from the technical and administrative perspectives. The Technical review consists of a DOB Plan Examiner (normally a P.E.) checking the plans and technical documents included in the application. The plan examiner formulates questions and objections from his review of the application (DOB form CD-9) and submits these to the applicant's engineer. The applicant in turn revises the application, modifies the submittal and resubmits it to DOB.

During the administrative review, DOB checks the application for completeness of the submitted items, processes the application fee, the data received entered into a database and checked for previous application for that crane model and configuration, and a Prototype-Number is generated for the crane.

Implementation of this recommendation should include the following actions:

- Manufacturers would satisfy predetermined, industry-standard criteria to qualify as an "Approved Manufacturer".
- Establish a simplified process for approving specific crane models and configurations.
- Determine criteria whereby the "Approved Manufacturer" loses such designation.

## **Manufacturers would satisfy predetermined, industry-standard criteria to qualify as an "Approved Manufacturer".**

The following list is proposed by the HRCO crane team, but should be reviewed and amended as necessary. Table C.6.1 contains some of the following in tabular form.

- 1. For the initial round of approval, the manufacturer should have at least two (2) different models of their cranes already proto-typed. This demonstrates a proven performance track record and a familiarity with NYC requirements.
- 2. The manufacturer is currently manufacturing the cranes included in the application or willing to support such going forward.
- 3. The manufacturer adheres to American or internationally accredited design and manufacturing standards and design practices, such as FEM, EN, DIN, ISO, SAE, AS, etc.
- 4. The manufacturer has an ISO 9000/90001 certification. The cranes that will be used in the Jurisdiction will need to be manufactured at an ISO 9000/9001 certified facility. The certifying agency should be independent from the manufacturer.

- 5. The manufacturer also comply to the ANSI crane standards (B30), or similar, when designing the cranes.
- 6. The manufacturer will send updates about safety recalls and bulletins to DOB at the same time as ones sent to the owners. This requirement will be for older models as well as new cranes. DOB will provide the manufacturer a list of the cranes already approved so they may be added to the recall list.
- 7. The manufacturer has a technical representative (engineer) in the US who will be the designated point of contact for all DOB communication. This representative will have enough technical background to answer most general questions about operating, maintenance and repair procedures for their crane products.
- 8. The manufacturer has factory-trained technician within a four hour travel window (ideally located in NY, NJ, CT or PA). This may be a different person than the technical representative.
- 9. The Manufacturer will provide the necessary manuals and technical information on the cranes in use today as well as the new ones. This documentation will include daily, monthly and annual inspection check lists for DOB to add to the third part inspection lists (C-R-03 Third Party Inspection).



10. Provide DOB access to manufacturer training courses for its inspectors when the manufacturer offers them (C-R-11 Training).

**Table C.6.1 – Manufacturer Criteria** 

## **Establish a simplified process for approving specific crane models and configurations.**

Once the manufacturer receives the Approved designation, they would still be required to submit an application for each crane and maximum configuration to be used in the Jurisdiction. This application would be similar to the one outlined in the current regulations (RS19-2) as this information is needed for DOB to perform some of their duties, such as, but not limited to:

Paragraph 3.1

- *1. Affidavit of compliance from the manufacturer as detailed in section 3.2 below,*
- *2. Operator's manual showing all configurations for which the engineer is seeking approval, general equipment specifications and manufacturer's recommended maintenance procedures.*
- *3. Load rating chart with chart number and page numbers for identification.*
- *4. Any supporting data, drawings, or calculations upon request.* **AND** from 3.2
- *5. List of all components: maximum boom length, maximum jib(s) length, maximum length of all other attachments,*
- *6. List of all counterweight combinations,*
- *7. List of standards used in the design of the boom and/or mast,*
- *8. List of standards used in the design of the jib and/or extensions.*
- *9. List of standards used in the design of the boom support system,*
- *10. List of standards used in the design of the counterweight support system and attachments*
- *11. List of standards used in the design of the rope.*
- *12. List of standards used in design of overturning stability.*
- *13. List of standards used in the prototype testing, and*
- *14. List of material(s) and material specifications used in the components listed in Numbered Items 3-7 above.*

DOB would process the application by primarily clerical means. DOB administrative staff would audit the submittal to ensure all the required documentation is included. If the package is fully compliant, then the crane would be granted approval status and given a proto-type number. If there is missing information, DOB would send an objection list to the manufacturer requesting the missing information.

### **Determine criteria whereby the "Approved Manufacturer" loses such designation**.

The HRCO crane team proposes that the following be used at a minimum.

- 1. The manufacturer fails to comply with any of the previous criteria.
- 2. There is a significant change in the operations of the manufacturer, such as
	- The manufacturer makes significant changes to the personnel in its design department.
	- The manufacturer out sources the crane design or the crane manufacturing to another company.
	- The manufacturer has a major change of management e.g. by merging with another company or being acquired by another company.

If the "approved manufacturer" status is revoked, the manufacturer should re-apply when such conditions are remedied. The cranes that have been previously approved would

maintain their Certificate of Approval as long as it was issued prior to the condition that caused the revocation.

# **C.6.2.3 Additional HRCO Data**

Presently, DOB reviews approximately 10 to 20 prototype applications per year. DOB plan examiners generally process the application within a few weeks of receiving information from the Engineer.

DOB has little if any direct communication with the manufacturers and rely on the Applicant's Engineer to address and answer objections or questions.

The HRCO crane team reviewed seven (7) applications for a Certificate of Approval (Table 6-2). DOB returned four (4) of them with objections and/or comments.



### **Table C.6.2: Proto-type Applications Reviewed by HRCO**

The following table shows the processing times of crane prototype applications. The average processing time for prototype applications was calculated as 110 days, beginning with the first submittal of the application and ending with the notification to the Engineer of Record (EOR) that the crane prototype was accepted. The date of application was supplied by DOB, and the date of acceptance is derived from the notification letters included in the prototype file.







To help explain the lengthy time frame, the HRCO team interviewed DOB personnel. The following issues were identified:

- Engineer of Record (EOR) supplied incomplete applications (see tables below) and then took time to answer DOB's objection points.
- In 2008, the prolonged times were also a result of DOB examiners spending time with the forensic teams on the two major crane accidents.

DOB and the HRCO crane team reviewed seven prototype applications. The average duration was 144 days from the submittal by the EOR to the approval. The results showed that DOB required 55 days and the EOR needed 89 days to address the objections and provide a complete set of documentation. Below are tables that outline these proto-type file reviews.



### **P391, - Amendment Liebherr LR1160, Crawler**

#### **P438, Amendment Liebherr 540 HC L12 Tower Crane**



#### **P446, - Amendment Liebherr LTC 1055-3.1, Mobile Crane Telescoping Single Cab**



#### **P502, Link-Belt 218 HSL, Crawler (Not Included In Final Calculation)**



#### **133 265 Ongoing**

#### **P506, National Crane 900 H, Boom Truck**





#### **P509, Liebherr 376 EC - H.12 Tower Crane**

**P510, Grove GMK 7550, Mobile Crane Telescopic Dual Cab** 



#### **P518, Link Belt RTC 8050 II Rough Terrain Crane**



The above prototype application list also shows that a large number of the applications are for cranes from leading manufacturers. These manufacturers would likely be among those initially submitting for the approved manufacturer process.

The HRCO crane team interviewed four of the primary manufacturers to determine their interest in an "Approved Manufacturer" designation. Their initial response was overwhelmingly supportive. They generally agreed with the criteria listed above and showed willingness to participate in the process.

In terms of benchmarking, there are only a few public jurisdictions that have specific crane model approval requirements. Below are the ones that have some form of crane approval prior to it being operated within their borders.

**Singapore** has approved twenty-one (21) models of tower cranes that may operate within their country between 2006-2008. This list also includes the approved configurations of these cranes. The stated objective is to "ensure that the tower cranes brought into use in Singapore meet the mandatory and regulatory requirements for safe operation.

The procedure is:

- The suppliers (manufactures or agents) or owners submits an application for the type approval of their tower crane using the prescribed application form and procedures describe in this document.
- The applicant must submit one application for each model of the tower crane for type approval.
- Upon successful application for the type approval, the department will issue a Type Approval Document for that model of tower crane.

The criteria that the agency uses comprise of the following items:

- The cranes must be designed to an internationally recognized standard (SS, ISO, EN, BSI, FEM, ANSI, DIN, ASME)
- The design must be verified by a third party inspection agency
- The manufacturer must put in place an accredited Quality Assurance System that is reviewed or audited periodically.
- The model shall meet the legal and procedural requirements, including but not limited to the provision of the safety devices/features as listed.

**Cal-OSHA** require that various cranes (tower and mobile) be designed to the ASME code written for that particular crane (Title 8, Subchapter7, group 8, §4884).

**New Zealand** Design verification is required for all cranes including second-hand cranes brought into New Zealand.

Two options are available for this process:

*(1) By Design Certificate:* 

 *Design verification by design certificate may be used for imported cranes from recognized manufacturers producing standard cranes, designed and built to an acceptable engineering standard* 

 *In all cases, where proven standard production model cranes are produced by manufacturers of established repute, subject to the following requirements, the crane can be accepted for design verification and fabrication inspection purposes on the basis of the manufacturer's design statement* 

 *The documentation required for design verification includes:* 

- *(a) A statement signed by the chief design engineer, or other person authorized (in writing) by the manufacturer to sign such documents, stating the standard that the crane was designed and built to and that an independent design verification has been carried out. This shall be to a standard acceptable to the Department of Labor, e.g. BS, AS, EN, ANSI, DIN, ISO, JIS, NZS and any others that may be gazetted at a later date (refer to Appendix C).*
- *(b) Sufficient data, drawings, documents and other information to readily identify the crane and all of its major components and parts supplied by the manufacturer or replacement parts that are authorized and approved by the manufacturer*

# **C.6.3 Recommendation C-14: Older Equipment**

*Require an extensive mechanical crane inspection every 10 years for all cranes and potentially an age limitation for operation in the jurisdiction.* 

## **C.6.3.1 Description**

As with most construction equipment, a crane and its components have useful lives. Using it past this time increases the risk of potentially hazardous failures. In a dense urban environment, this places many people at risk within the potential crash zone of a tower or large mobile crane.

An age-survey of the active cranes in New York City indicates that 41% of tower and 10% of mobile cranes are older than 20 years and 23% of tower and 9% of mobile cranes are older than 30 years. This recommendation proposes heightened inspections and possible age limitations to address this concern.



**Figure C.6.1: Example of Older Equipment (Site 48)**

# **C.6.3.2 Recommendation Approach**

The goal of the proposed 10-year inspection should be the evaluation of all safety related and load bearing components to assess their condition and to assure a safe operation until the next inspection of the component takes place.

An inspection plan/checklist indicating the items to be inspected and the type of inspection (e. g. "visual", "measurement and comparison to manufacturer recommended values" or "NDT") should be prepared by the following entities, in order of preference:

- 1. The Original Equipment Manufacturer (OEM).
- 2. A qualified OEM distributor or OEM local representative with a letter of the OEM delegating this type of service work to the distributor or representative.
- 3. A Professional Engineer with experience in crane inspection if the OEM is not available.

Details of the inspection plan could include the following as well as any additional items that the above requires:

- Measure the turntable / slewing ring play in several directions and compare these with the OEM specified tolerances. If any measurement fails to meet the OEM minimum specifications or if such specifications are not available, the slewing ring should be repaired or replaced.
- Removal of at least 20 % of the slewing ring fasteners. These should include, at a minimum, the upper bolts in the boom/jib or counterweight/jib direction. These are visually checked for possible elongation and subjected to nondestructive testing (NDT), if there are any signs of cracking or elongation, all slewing ring fasteners must be replaced. As an alternative, all slewing ring fasteners are replaced without checking.
- Disassembly of all gearboxes for hoist and boom drives and brakes, if their components are not visible from the outside. Visual inspection and checking for wear of components like bearings, shafts, axles and gears. NDT or replacement of components, which would cause the load to slip or fall (e.g. various shafts, brake disks, gears, brake actuators).
- Inspection for wear and fatigue of all valves and hydraulic motors that hold, bear or control load movement and braking, and calibration and functional testing of these components after reassembly.
- Hydraulic cylinders should undergo a load holding test for at least 30 minutes to test for creep and leakage.
- All hydraulic hoses should be checked for signs of wear or deterioration and replaced if warranted.
- Sheaves and sheave bearings should be checked for wear and replaced if warranted.

- Telescoping booms should be disassembled to allow inspection and NDT of interior components and boom parts that are hidden in normal operation.
- All relay contacts, cable terminations, wiring, electrical components and enclosures should be inspected for worn / damaged insulation, signs of heat/burning and possible water ingress.
- Load bearing bolts and pins should be removed for inspection and subject to NDT.
- All load measuring devices should be recalibrated.

All components with defects or issues must be replaced or repaired as recommended by the OEM (see C-R-06, Repair and Maintenance). The reassembled crane must be load-tested with 100% rated load including all moment and a load holding test, including each outrigger (see C-R-15, load testing). For mobile cranes any overload warning devices should be tested as recommended by the manufacturer or the Engineer of Record.

This 10-year window for extensive inspection could provide an approach for identifying the "useful life" of a crane. A qualified inspector (see C-R-03, qualified inspector) would submit a detailed report of the inspection (including replacement part list) to DOB. This report would include a statement that the crane is fit and for safe operation and a set of conditions and requirements set by this inspector for the Owner to follow until the next major inspection. Some of these conditions and requirements may include:

- A change in the routine inspection schedule
- Special inspections at designated time intervals
- An extensive inspection at an earlier date than 10 years
- Install a device to count load/stress cycles

If the qualified inspector cannot provide this program for continued use, the crane would be deemed to have reached its "useful life", and removed from service in NYC and the crane's CD revoked.

Both NYC and OSHA require various crane components be inspected on frequent and periodic bases. These inspections are primarily exterior, visual inspections or exterior NDT inspections performed on directly accessible components or ones that can be accessed with minimal preparation. Some safety related or load bearing components are hidden from a visual inspection. These are subject to wear and fatigue.

Most crane manufacturers recommend long term inspection and maintenance requirements for components either in their manuals or when requested by the crane owner. There is no industry standard or a scope of long term inspection requirement specified by DOB.

Figure C.6.2 provides a tower crane age analysis that were in operation 1/29/09. In summary, 17 out of 34 tower cranes (50%) are more than 10 years old, and 23% are older than thirty (30)

years. The tower cranes over 30 years are primarily FMC TG1900 (62.5%) and Favco Model STD 1500 (37.5%).



**Figure C.6.2: Tower Crane Age Distribution** 

Figure C.6.3 shows the age of mobile cranes registered with a NYC CD (certificate of operation). The results show that 209 out of 593 mobile cranes (35%) are more than 10 years old, and 9% are older than thirty (30) years.



## **Figure C.6.3: Mobile Crane Age Distribution**

The relationship between the increased potential for equipment failures with increasing age can not be ignored. Recently, a crane suffered an equipment failure that caused an abrupt drop of the load (a concrete bucket reportedly weighing approximately 15,000 lbs). The cause of the failure was a worn drive shaft (see Figure C.6.4). The crane and the failed component were reported to be over ten years old. This component is not accessible to observation without a detailed inspection procedure as outlined above.



**Figure C.6.4: Worn Pinion and Pinion Spine**

## **C.6.3.3 Additional Considerations for Good Practice**

**The initial application for a certificate of operation for a used crane should require a statement by the manufacturer or its distributor that the crane still receives manufacturer support. DOB should not allow the registration of used cranes which are not supported by a manufacturer.** 

Age limits and manufacturer support are not included in DOB requirements to receive a certificate of operation (CD) for a used crane. All that is currently required is for the crane to have a valid a prototype certificate and pass the inspection.

Manufacturer support is extremely important for all cranes, and becomes even more critical for aging equipment. Reasons for this include:

- 1. Manufacturers provide service bulletins regarding performance issues that arise with cranes that are in operation.
- 2. Manufacturers are the most appropriate source for information on conducting repairs or retrofits to aging equipment.
- 3. The manufacturer is in the best position to assess the intended service life of a crane and its components based on their original design.

**A study should be undertaken to determine the role of fatigue as it relates to useful life of cranes.** 

Steel structures, which are subjected to stress fluctuations or reversal, are subject to fatigue. As such, cranes designed in Europe use engineering standards that require the manufacturers to use formulae that calculate specific fatigue strength based upon the projected stress cycles. It is not unusual for a manufacturer to perform such calculations, but they are generally deemed proprietary and not available to the public.

If the number of stress cycles is exceeded, fatigue cracks will eventually start to appear. If these are not detected and repaired between when they first appear and the time of "rapid crack growth" the component will fail. With increasing fatigue this time window becomes shorter. There is further discussion of this in "Fatigue Design Basis" section.

DOB should work with the industry and manufacturers to determine the useful life of a crane or of their components via an engineering based approach. Consideration should be given to the fact that cranes in NYC often operate in densely populated and high traffic areas placing many people at risk that live and work in the potential crash zone. There is further discussion of this in section C.6.3.4.

There is currently no age limit on cranes operating in NYC. The industry replaces cranes for reasons including increased maintenance cost, decreased reliability, obsolescence, and/or higher productivity of newer equipment.

The NYC DOB requires Owners to subject the tower mast, jib and booms sections to NDT prior to the tower crane being assembled. In these inspections, tower and mast sections are rejected for a failed test. One such mast section was rejected when 2 out of 8 foot plates failed the NDT (Site C-95).

In various meetings with DOB, HRCO staff and manufacturers, manufacturers did not provide information regarding the useful life of their equipment. One representative maintained that a crane could have an "infinite" life but qualified this by noting that inspections and on-going maintenance and repair are necessary in assuring safe crane operation and that the frequency of required inspections and repairs will increase with the age of the crane.

Within the scope of the current investigation, the HRCO team could not collect sufficient information to establish crane retirement based on age or other criteria (such as inspection results or service history). A further investigation of this topic is required.

During the course of the HRCO investigation, one specific crane model became the source of investigation for fatigue-related failures. Investigations by DOB were on-going at the time of preparation of this report, so detailed findings were not available to the HRCO. But, as reported to the HRCO crane team, multiple cranes of the same model exhibited similar fatigue crack development.

The findings of such failure studies, which would differentiate between systemic and localized issues, should be used as the basis for assessing the risk of specific crane models and determination of conditions for their operation in the jurisdiction.

## **Cranes that lack certain design safety features should be updated with appropriate components to meet the newer standards or not be used in the city.**

Older cranes generally have less advanced safety features. However, to equip the older cranes with some updated components may require a major rebuilding effort.

A common short-coming of older design is the limited access to the outermost tower bolts. In order to reach them, riggers must climb onto a platform that is attached to the outside of the tower. This platform is lifted into position on the outside of the tower using the crane and its position must be detached and reattached with each climbing section. In addition the tower crane rigger often has to change hook points for his safety harness. On 9/4/08 (Site C-94), an experienced tower crane rigger fell from a detachable, crane suspended work platform and died. A few weeks later on 11/12/08 (Site 49) the HRCO team witnessed a similar situation where a rigger climbed onto such a platform without a harness.

Newer tower cranes utilize different tower designs. This design does not require the worker to ride the load, and he can remain on a platform to change pick points during assembly, climbing or dismantling process. Tower bolts can either be reached without the use of an outside platform or a platform which remains attached to the climbing frame. This minimizes the danger of a fall or of being crushed by suspended loads (figures C.6.5 and C.6.6).



**Figure C.6.5: Riggers "Riding the Load" Figure C.6.6: Rigger Kicks** 

**Platform to Free It** 

On older mechanical mobile cranes, the different hoist drums for the boom and load hooks are driven by a single combustion engine. Using friction couplings, the different hoist drives are engaged or disengaged from the main engine by the operator while the engine is running. In addition, the operator must engage/ disengage the hoist brakes for the different hoists to move the particular hoist drum. The process of releasing the brake and engaging the coupling must take place at the same time without any jerking movement requiring skill from the operator (similar to starting up a car with a manual transmission on an incline).

It is extremely difficult to install a safety device that automatically shuts down a hoist drum or boom drum on this type of crane. Newer cranes with hydraulic or electric drives automatically stop hoisting or booming (e.g. in case of two-blocking which could cause the boom or jib to break) when the load moment becomes too large (danger of tip over) or when the maximum line pull force is reached. With the older mechanical cranes these safety aids can only give an acoustical and optical warning to the operator

On 7/21/05, the boom of a mobile crane with mechanical transmissions broke off, because the operator's foot slipped off a foot-pedal that caused a jerking hoist-drum movement. With newer hydraulic or electric cranes, acceleration and deceleration of components are dampened either by limiting valves or by more sophisticated control mechanisms so that a brief abrupt movement of the controls is less likely to create shock loading on the crane's structure*.* 

DOB grandfathered older cranes when it made certain safety aids mandatory (for instance, anti two blocking sensors for the Manitowoc 4100). In other cases DOB demanded retrofitting. There were two instances (3/9/05 and 6/29/07) where a grandfathered crane did not have an anti-two block device resulting in damage to the crane.

Therefore, primary items to consider would be:

- Larger mobile cranes (those that require a Certificate of On-site Inspection) should include features that automatically stop hoist or boom movements when an operational aid alerts the operator of a potentially risky situation. This includes but is not limited to:
	- o Anti two blocking device,
	- o Load moment monitoring devices (having a rated capacity limiter instead of a load and/or capacity indicator).
	- o Maximum and minimum boom automatic angle shutoffs (instead of stops only).
- Tower crane designs should minimize the situations where the tower crane riggers must "ride" a suspended load or work on platforms suspended from the crane hook.

## **C.6.3.4 Additional HRCO Observations**

There are a few public jurisdictions that require either assign a useful life or require more indepth inspections as crane age. Below are the ones that have attempted to address this area.

**The Australian** standard 2550 (Cranes, Hoists and Winches – Safe Use) requires that cranes and lifting equipment undergo a Certification and Refurbishment when they have reached the end of their design life, (or where this is unknown after 25 years for the structure and 10 years for the mechanical). This includes a major inspection to assess their suitability for continued safe operation.



**Singapore** limits the service life of mobile cranes per the following schedule:

Cranes exceeding the maximum service life need a "thorough assessment" by an approved  $3<sup>rd</sup>$  party agency and approval by the MOM ("Ministry of Manpower" agency regulating construction work safety). This includes a proposal detailing *"Usage Patterns (e.g. number of operating cycles per hour at certain load condition)"* and a *"proposed scheme to evaluate the remaining service life of the crane"* including "*The methodology and assessment employed including testing and inspection to be carried out to address potential fatigue stresses experienced by the crane"...* 

Singapore limits the service life of tower cranes per the following schedule:



**New Zealand** regulations include the following: "*As the end of the national design life of a crane approaches… at periodic intervals or when a second-hand crane is imported into New Zealand, inspection and testing shall be carried out in order to determine that the crane will remain safe for continued use.* … *If there is insufficient information to enable the equipment inspector to make a proper assessment of the condition of the crane, the inspection body shall not certify it* 

## **Fatigue Design Basis**

Europe addresses fatigue of a crane's metal structures by using the number of stress cycles a particular component undergoes. The service strength of a steel structure is influenced by the quantity (number) of stress cycles, the magnitude of the stress range, notch effects and steel grade.

The European standards classifies fatigue design of tower crane components relative to anticipated stress cycles ranging from 600,000 to 1.5 million. The stress magnitude is determined by the full stress range experienced by a component as it cycles from compression to tension and variations between the two. Finally, they consider the notch effect, which is a function of the shape, structural design, hole pattern or type and quality of the weld.

Depending upon the magnitude of the above, the allowable stress on a steel structure is reduced accordingly. The fatigue stress on the crane is introduced by repeated lifting and releasing loads and slewing of the crane. Wind influence is not considered when calculating fatigue.

As equipment approaches the service life (or fatigue limit) very small, and perhaps undetectable flaws, can grow at a rapid rate to a critical crack size that could cause failure. Procedures exist to estimate the number of cycles required for a flaw to propagate to a critical crack (one such is the Paris equation). This parameter of crack growth rate is necessary to determine the inspection interval that would be necessary for a crane that could be operating beyond its fatigue life.

Thus the essential logic for fatigue analysis of a crane involves:

- 1. Establishing the original fatigue design basis of the individual crane components (number of cycles and stress magnitude).
- 2. Determining the actual number of cycles experienced by a specific crane component. This could be accomplished in the future by mating data loggers ("black box") with component tracking. In the absence of such technology, it requires estimates of cycles. A crane in steady use might accumulate on the order of 600 cycles per week, or 30,000 cycles per year.
- 3. Comparison of the actual service history with the design basis provides a measure of remaining life. It should be noted that this assumes the crane has been properly operated and has not been significantly overstressed – in which case the fatigue life could be significantly reduced. The application of data logging technology could serve to provide insight into whether crane components had been overstressed.
- 4. As a crane component approaches the fatigue limit there is an increased potential for relatively rapid development of fatigue cracks. At this point, the component could either be removed from service or, in theory, carefully monitored for crack development. Monitoring would require a determination of how quickly a crack could grow from

undetectable to hazardous. The inspection method and frequency would then need to be sufficiently conservative to ensure identification of fatigue crack growth at its early stages.

### **Airline Industry**

The airline industry has recognized for many years the importance of applying stricter maintenance and repair systems on aging aircraft.

For the commercial aviation fleet, Congress passed the Aging Aircraft Safety Act of 1991 to address aging aircraft structural concerns resulting from the April 1988 accident involving a Boeing B-737. This noted failure (Aloha Airlines flight 243, NTSB Report # AAR-89/03), which was caused in part by fatigue issues, precipitated an overhaul of maintenance and repair procedures for aircraft. The commercial airline industry has an advantage over construction cranes in that the record keeping is far more advanced. For example, after the failure of Flight 243, the FAA was able to release flight restrictions and inspection requirements specifically for B-737's with more than 30,000 landings, because detailed flight information was available from which to identify an age threshold at which planes might be at risk. Similar operational data, with which to establish the functional age of cranes and crane components, is not currently available.

Similar attention is being paid to aging aircraft in the general aviation fleet (typically smaller, private aircraft). Two aspects of best practices are currently being promulgated by the FAA: Airplane Record Research and Special Attention Inspection. Airplane Record Research provides a basis of information by compiling flight histories for the specific aircraft combined with operational records for its make and model. Special Attention Inspection recognizes that normal annual inspection may not be sufficient for aging aircraft and that more detailed inspections and rehabilitations may be needed to keep the aging aircraft at an acceptable level of reliability.

## **C.6.4 Recommendation C-21: Electric Tower Cranes (Further Study)**

*Have an all-electric tower crane fleet in the jurisdiction by a specified date.*

## **C.6.4.1 Description**

Electric crane use is increasing for a multitude of reasons including environmental concerns and cost of operation. While those considerations are outside of the scope of the HRCO study, some aspects of electric crane use could positively impact crane operations in New York relative to safety. Thus, if there is a general move toward electric tower cranes, the HRCO crane team supports this for the following reasons:



**Figure C.6.7: Electric Crane Figure C.6.8: Diesel Hydraulic Crane** 

- **Provision of a modern crane fleet**. This is the primary benefit of moving to an all-electric fleet. This would provide an opportunity to phase out older equipment lacking modern safety features.
- **Removal of refueling operations**. A typical diesel crane uses up to 10 gallons of fuel per hour and requires refueling every few days. This usually requires hoisting drums or tanks of fuel to the machine platform. This presents a very small but obvious risk of hoisting and handling flammable substances.
- **Electric cranes require less hydraulic fluid.** The primary reason is that the diesel machines require the fluid for their hoist drives, while electric cranes normally have a small amount of hydraulic fluid used in brakes and the climbing frame cylinders. There were two leaking incidents in NYC while the HRCO team was on assignment, both involving the same crane. The first one the HRCO team observed while investigating a crane (see Figure C.6.9), and the second time a hydraulic fitting failed and hydraulic fluid spewed into the street below requiring a HazMat response and clean up.
• **Diesel crane engine noise levels exceed 90 dBA**. Electric cranes operate at less than 80 dBA. This is a significant difference, relative to hearing health, for anyone working in vicinity of the crane.



**Figure C.6.9: Leaking Hydraulic Fitting** 

### **C.6.4.2 Recommendation Approach**

The final time frame should be selected so as to provide sufficient notice to owners and operators so they may adjust their crane usage and fleets.

A number of logistics would need to be investigated for this recommendation. For example, electric cranes require an electrical power source. Most buildings should have sufficient power from the electrical grid by the time the tower crane arrives on site. But, this will require some coordination between the user, the City and the electric company.

# **C.6.5 Recommendation H-1: Hoist Equipment Acceptance (Further Study)**

*Create and implement an Equipment Acceptance Certification program for hoisting equipment employed in the NYC area.* 

# **C.6.5.1 Description**

There is no current requirement, or standardized quality assurance program to ensure hoist equipment in use in NYC is in compliance with standard industry quality assurance practices for design, manufacture, materials, testing, and that it is in compliance with all applicable regulatory specifications. This recommendation proposes an Equipment Acceptance Certification that would require Hoist Contractors to certify that the equipment employed by them has satisfactorily passed minimum quality requirements.

For the most part the hoist industry is not required to provide or record quality assurance information for their equipment and as such they typically don't require it from their suppliers. Contractors will simply buy a hoist, mast, or mechanical drive parts without requiring quality assurance certifications. Additionally, some contractors manufacturer their own equipment but not necessarily with any specific quality control program in place.

During the course of this study the HRCO hoist team visited 6 hoist contractor facilities. All of them but one performs some form of fabrication or major repairs. Aspects of contractor QA/QC procedures are summarized in Table C.6.3 and discussed below.

Of the five contractor facilities that have shops for fabrication and repair, only two maintain some manner of quality control program. These two facilities have extensive operations, performing major modifications to their cars and mast sections (one facility even fabricates their own mast sections). Quality procedures at these two facilities include:

- quality inspections on the mechanical drives and rebuild or repair any defective parts
- mast sections are UT tested and have identification numbers for traceability
- in-shop testing of assembled cars (including drop tests)

However, neither actually has a formally documented quality control program.

A third contractor had no quality control program, though they do perform UT and then tag tested sections but only at the client's request. They also perform car testing in shop.

The remaining 2 of the 5 contractors that perform fabrication and repair work exercise very little quality assurance. One of them makes major repairs to the majority of their mast section inventory without qualified welders. The welder observed by the HRCO hoist team was not AWS or New York State certified. This contractor also did not have the means to shop test their cars, although there were at least aware of the potential for internal corrosion of mast legs perform UT testing before returning them to service.

None of the contractors required quality assurance information from the suppliers and manufacturers that they buy their equipment from. And although many of them are buying premium products from established manufacturers, just as many are buying "cloned" products.

### Cranes and Hoists C-38

One contractor purchases less expensive "cloned" equipment and then rewires the entire car to meet UL standards, removes and replaces floor plates and cage, and removes and replaces the gearing in the drive. They claimed that after one installation with the "cloned" parts, the gears wear out. So they replace them with a German made product from the outset.





### **C.6.5.2 Recommendation Approach**

Hoist contractors would certify that equipment in service meets or exceeds specific criteria. The criteria could include:

- 1. Design of such equipment has been performed by a qualified engineer, for example, as demonstrated by a minimum of 10 years experience in the design of similar type equipment.
- 2. Manufacturer of equipment is certified to a relevant quality assurance program (e.g. AISC certification). The quality program should be documented in a manner that can be submitted to DOB.
- 3. All weld procedures, including weld process qualification reports (WPQR), weld materials, weld process specification (WPS), and welder qualifications, must be in accordance with AWS D5.1 or D5.5, as required.
- 4. All materials are as required by design and are mill certified.
- 5. Product testing is to be performed on all products to confirm load ratings.
- 6. All in-service equipment must be in its original manufactured configuration. Any parts that are replaced or repaired must meet Original Equipment Manufacturer (OEM) standards.
- 7. Gearing, bearings, shafting, brake liners, housings, cable, rollers, limit switches, must all be by original OEM products or be by approved manufacturers.

# **C.7 SITE SPECIFIC DESIGN**

# **C.7.1 Description**

This section addresses issues that relate to the overall site design of tower and large crawler cranes. This includes foundations for tower and crawler cranes and building tie-ins for tower cranes. Many times these site-specific design elements are altered during crane erection due to unanticipated site conditions.

Recommendations for tie-ins and foundations serve to expand and strengthen engineering efforts by crane and building engineers as well as DOB plan examiners. No matter how well designed, manufactured or maintained, if a construction crane is not properly supported, it could be subject to catastrophic failure.

Tower and large mobile cranes rely on counterweights to support lifted loads. Proper configuration of the counterweights (as well as general functioning of the crane) is confirmed by a load test prior to putting the crane into service. Recommendations for load tests and counterweights primarily take practices already recommended in standards and by manufacturers and formalize them for NYC.

The further study recommendation for wind loading is related to the understanding that local wind loads in urban environments can vary significantly from standard wind load charts. A related recommendation for high-rise concrete calls for increased monitoring of actual wind speeds in Manhattan. Data from this study should be used to assess the appropriateness of current crane design wind speeds.

The hoist recommendation for engineering sign-off calls for a formal review of the ability of the building to support loads imposed by the hoist equipment.

# **C.7.2 Recommendation C-8: Tie-Ins**

*Tie-In connections should be subjected to special inspection and require improved design and erection procedures.* 

### **C.7.2.1 Description**

Tie-ins are used with tower cranes that exceed the maximum freestanding tower heights set by the crane's Original Equipment Manufacturer (OEM). In such instances, the crane tower is usually attached to the building being constructed. The tie-ins transfer the lateral reaction forces of the tower crane to the building structure. Their placement, location and design are specific to each application and are prepared by the OEM or the Engineer of Record. Tie-in design, calculation and installation are approved by DOB as part of the "Certificate of On-Site Inspection" [CN].



**Figure C.7.1: Examples of Tie-ins (Site C-10)** 

### **C.7.2.2 Recommendation Approach**

Implementation of this recommendation should include the following actions:

- The connection at the building's floor slab should be subjected to Special Inspection for conformance with the approved drawings.
- If using friction connections, the crane Engineer of Record must specify the required bolt torque to providethe necessary clamping forces between the steel tie-in foot plate and the concrete slab are included in the design.
- If using a bearing connection, the crane Engineer of Record and the contractor should check that the bolt holes in the concrete have a close tolerance, and the bolts/threaded rods should be pre-tensioned. An alternative is the use of grout or steel bushings.
- Permitting of crane and hoist machines should require PE sign-off for loads imposed.

### **The connection at the building's floor slab should be subjected to Special Inspection for conformance with the approved drawings.**

This inspection would include photographs showing the rebar-placement and documentation of the inspection in a log available to DOB. For installations that require higher-strength concrete at the tie-in locations than in adjacent regions of the floor slab, the contractor should supply test results, to the Special Inspector, verifying required concrete strength.

Tie-in design and installation are covered under Chapter 33 of the New York City Construction Code, and more specifically paragraph 3319.6 requires the equipment user, or his designated representative, to apply for and obtain a certificate of on-site inspection that DOB must approve prior to a crane arriving at site. DOB presently does not require Special Inspection of, or typically inspect, the tie-in locations prior to pouring concrete.

One occurrence was noted where the concrete design strength was higher than the installed strength. This was confirmed by the Crane EOR, and the EOR provided calculations that the lower installed strength was acceptable based upon the design criteria. If the original design was correct, the concrete may have failed. There was also an occurrence where the building EOR added rebar to the Crane EOR's design to overcome the bending moment on the concrete slab (site C-110 4/7/09). Figure C.7.2 shows the addition to the Crane's EOR drawings and the building EOR stamping the drawing.



**Figure C.7.2: Tie-in Slab Drawing Modifications (Site C-110)** 

### **If using friction connections, the crane Engineer of Record must specify the required bolt torque to provide the necessary clamping forces between the steel tie-in foot plate and the concrete slab are included in the design.**

The crane user must provide a means to assure that the bolt connections remain properly torqued (e.g. periodic re-torquing of bolts). Re-torquing may need to be conducted on a weekly, or even shorter, basis. Documentation of the minimum bolt torque and re-torquing procedure must be kept on site and accessible to DOB. The HRCO crane team recommends that the EOR insert such on the drawings provided with the Certificate of On-Site Inspection (CN).

There are two primary professional engineering firms that submit applications for Certificates of On-Site Inspections for tower cranes. One prefers to design a friction connection and one a bearing connection. The friction connection relies on the clamping forces and smaller bolts to hold the tie-in strut in place during the crane's operation. The reason the user must check the bolt for looseness is that the steel will have a tendency to wear down the concrete.

The HRCO crane team found four (4) instances where there were loose bolt(s) on 3 friction connections, and one of these showed signs of tie-in movement (see Table C.7.1).



 **(Site C-55, 1/5/09)** 

**Figure C.7.3: Examples of loose friction tie-in strut connections** 

**If using a bearing connection, the crane Engineer of Record and the contractor should check that the bolt holes in the concrete have a close tolerance. The bolts/threaded rods should be pre-tensioned. An alternative is the use of grout or steel bushings.** 

This is one of the preferred tie-ins designs submitted by the EOR's in New York City. The bearing connection uses larger bolts and relies on the allowable bearing pressure of the concrete.

The ability to check a bearing connection is limited to when the crane is dismantled. The HRCO crane team observed one instance of a bearing connection with loose bolts (see Table C.7.1).



**Figure C.7.4: Friction Connection Bolts (Site C-88 – 1/5/09)** 





### **Require the building engineer of record or an engineer acceptable to DOB to review the plans to determine the building can support the loads imposed by the crane.**

The procedure would require the following to be submitted to DOB:

- Building structural information submitted by the building Engineer of Record with currently available information to support an analysis of loads imposed by the crane equipment (if available for existing buildings).
- An analysis of the loads imposed by the crane equipment (considering at a minimum, local resistance of reaction forces and lateral system analysis) by either the building Engineer of Record or by a licensed professional engineer acceptable to the Department of Buildings. The reviewer should document this by a signed shop-drawing stamp on a copy of the approved tie-in drawing**.**

DOB has examiners that review each application for compliance to the regulation and they check the calculations provided by the licensed engineer. The examiners require the crane licensed engineer to provide the calculations of forces created by the crane. Generally, the building engineer has not signed off or stamped the crane drawing indicating that the building and slab can withstand the forces.

A review of 14 open CN's showed only four contained such a letter or stamp from the building (or independent) engineer (see Table C.7.1). On one of these occurrences, the building EOR added rebar to overcome a bending moment in the slab (Site C110).

# **C.7.2.3 Additional Considerations for Good Practice**

**Climbing frames should be stored at all times in accordance with manufacturer recommendations (typically this is at the top tie-in). The Site Safety Manager or similar personnel should receive specialized training and tools allowing them to supervise loosening of tie-ins as required in case of a storm warning.** 

Presently, only a Master Rigger can supervise all aspects of the assembly, climbing or dismantling of a tower crane. The HRCO crane team observed one occurrence in which the plans lacked detailed information regarding the releasing of a tie-in.

Some site drawings prepared by the engineer of record require that in cases of an upcoming storm condition certain tie-ins must be loosened and/or the climbing frame lowered and secured at the top tie-in. In New York City, only a licensed master rigger and properly trained crew are allowed to perform these operations.

There may be, at any one time, at least 20 cranes requiring these storm preparations located within the jurisdiction. This could put extreme pressure on the limited number of licensed riggers that can prepare the cranes properly. The engineer of record should prepare the loosening procedure and provide training and instructions for specific tie-ins.

### **Tie-in installation should be done only when the crane is in a balanced position. This will assist in the event where a tie-in must be released and re-installed.**

Installing ties while the crane is "balanced" (i.e. the crane is configured to minimize the overturning moment) minimizes the force in the tie. In this way, if the crane is returned to the balanced position when the tie needs to be released the unbolting process will be much easier. This is a particularly beneficial in case a tie must be released in an emergency situation such as a high wind alerts.

### **Require positive steel rope or steel structure support from the tie-in collar to the tower leg.**

It is common practice to attach wire ropes from the tie-in collar to a mast section/leg as a safety should the primary collar attachment to the tower via shims, threaded friction pads or similar means come loose.

At two installations the safety sling for the tie-in collar was attached to a horizontal member (Figures C.7.5 and C.7.6). This introduces a bending moment on a tension or compression member that is normally not designed for bending.

### **If the tie-in collar is not close (as defined by the manufacturer) to a panel point on the tower section, the tower-legs should be reinforced or inner bracings installed in accordance to the manufacturer's recommendations.**

Engineers of record typically design the crane installations with the tie-in collars at panel points or note that reinforcement of the mast section is required. This is a good practice that should be promoted (Figure C.7.7). Safety slings attached to tower lacings



**Figure C.7.5: Safety Slings at Site C-62.** 



**Figure C.7.6: Safety Slings at Site C-73.** 



The circled beam is an example of inner-bracing near the collar

**Figure C.7.7: Example of Tower Reinforcement at Tie-in (Site C-78, 10/9/08).** 

# **C.7.2.4 Additional HRCO Data**

Several jurisdictions and national standards have regulations that specifically speak to verifying the appropriate loads for tie-ins. Table C.7.2 provides a summary of a few.

<b>Standard or</b>	<b>Covered Issue</b>		
<b>Jurisdiction</b>			
<b>ASME</b>	Tie-in must be designed and anchored to the collar by a qualified person pursuant to the forces provided by the manufacturer		
	A qualified person shall review the transference of the horizontal and vertical crane reactions to the building		
	The concrete strength must be at design prior to climbing a crane		
	A qualified person shall review the integrity of the host structure for the effects of crane, load, and wind forces at each level of the structure		
	The user must check for looseness or preload for the connection after the first day and the first week of operation and then monthly		
Construction Safety Association of Ontario	The shoring and bracing that support a tower crane or tie it in place shall be designed by a professional engineer in accordance with the crane manufacturer's specifications		
	The structural engineer responsible for the structural integrity of the building or structure shall review the design drawings for the foundation to ensure the structural integrity of the building or structure		
C-DAC - OSHA	Prior to, and during, all climbing procedures, the employer shall: (ii) Have a registered professional engineer verify that the host structure is strong enough to sustain the forces imposed through the braces, brace anchorages and supporting floors		
	The following additional items shall be included (inspected): (ii) The upper- most tie-in, braces, floor supports and floor wedges where the tower crane is supported by the structure, for loose or dislodged components		
Health and <b>Safety Executive</b> - Britain	A report prepared by appointed person that planned and supervised the erection of the tower crane. The report should include: • Tie loadings; • Confirmation from the building designer (Structural Engineer) that tie loadings to be imposed on the building can be absorbed by the building structure; • Confirmation that the tie design, type and fixing method is sufficient for the anticipated tie loadings; • Confirmation that the ties have been correctly assembled positioned and adjusted.		
Hong Kong	Requires that the structural design of the building is the responsibility of a Registered Structural Engineer. This includes that all anchorage points be designed to withstand maximum loads that the crane may exert in the most severe static and dynamic conditions.		

**Table C.7.2: Summary of Other Jurisdiction and Standards Related to Tie-ins** 

# **C.7.3 Recommendation C-9: Foundations**

*Foundations should be subjected to special inspection and require improved design and erection procedures.* 

# **C.7.3.1 Description**

Concrete foundations for tower cranes are typically poured together with the building's foundation, and prior to the application for the Certificate of on-site Inspection (CN). This results in the foundation being installed without notifying DOB or providing DOB the opportunity to inspect the installed anchor stools and rebar mat to ensure they are in compliance with the approved drawing(s). At present, there is also no formal provision for Special Inspection of the foundation system.

The industry typically uses a template to align the anchor stools. A non-rigid or insufficiently fastened template may shift during the pour. If this occurs the contractor will need to elongate the bolt holes and/or shim the anchor stools to mount the first tower section.



**Figure C.7.8: Tower Crane Foundation (Site C-3, 9/5/08)** 

### **C.7.3.2 Recommendation Approach**

Implementation of this recommendation should include the following actions:

- The Crane Engineer of Record (EOR) should submit foundation plans to DOB prior to pouring; and in addition to structural details of the foundation anchorage, the plans should identify any issues and conflicts with known site conditions
- Require Special Inspection before the foundation pour to confirm conformance with design drawings. To facilitate this, the crane user should notify DOB at least 48 hours prior to the foundation pour to provide opportunity for DOB to audit the installed condition.
- Allow the crane installation contractor to use an actual tower mast section to assist with the alignment of the anchor stools by casting the stools into the foundation while attached to the section. If a template is used, it must satisfy ANSI B30.3 requirements. If a mast section is used, the Contractor should request DOB to perform a pre-assembly inspection for the installed section.
- The crane user should install Original Equipment Manufacturer anchor stools whenever available.

### **The Crane Engineer of Record (EOR) should submit foundation plans to DOB prior to pouring; and in addition to structural details of the foundation anchorage, the plans should identify any issues and conflicts with known site conditions.**

The typical foundation design and construction process (particularly for crane foundations that fall within the foot print of the new building) involves the following:

- The tower crane foundation is designed by the crane Engineer of Record (EOR) and constructed in conjunction with the building foundation.
- The process typically occurs weeks or months in advance of selecting a specific tower crane make and model.
- The EOR designs the crane foundation to accommodate the worst-case loads from probable crane models.
- Adapters are used, as necessary, to mate the final crane selection to the existing foundation.

Once the contractor decides on a particular type of crane, he applies for a Certificate of On-Site Inspection sending plans and calculations of the

foundation to DOB. As identified above, DOB reviews the plans for the foundation as part of the certification process.

The HRCO team noted instances where the foundation was poured prior to the CN submittal. NYC crane industry representatives confirmed in DOB industry meetings, that this is commonplace.



The foundation is poured and the rebar placement cannot be checked.

**Figure C.7.9: Poured Foundation (Site C-78, 8/7/08)**

On one occasion, the foundation was poured while the plan examiners were reviewing the application. In this instance, the contractor attempted to epoxy dowels in concrete just 2 days after it was poured without consulting the epoxy manufacturer. DOB discovered this due to an inspector being on-site for another reason and stopped the job until the epoxy manufacturer was consulted (Site C-78).

Foundation design and eventual installation are covered under Chapter 33 of the New York City Construction Code, and more specifically paragraph 3319.6 requires the equipment user, or his designated representative, to apply for and obtain a Certificate of On-site Inspection that DOB must approve prior to a crane arriving at site.

**In order to better ensure that the established technical requirements are being followed, the Department should require a Special Inspection before the foundation pour to confirm conformance with design drawings. To facilitate this, the crane user should notify DOB at least 48 hours prior to the foundation pour to provide opportunity for DOB to audit the installed condition.** 

Special Inspections have not been required. However, the industry has performed some at their own discretion. Proper crane foundation construction is critical for the support of the crane, particularly the initial period of use when the crane is free-standing. Special inspection is clearly warranted to provide assurance of proper construction.

### **Allow the crane installation contractor to use an actual tower mast section to assist with the alignment of the anchor stools by casting the stools into the foundation while attached to the section.**

If a template is used, it must satisfy ANSI B30.3 rigidity requirements. If a mast section is used, the Contractor should request DOB to perform a pre-assembly inspection for the installed section*.*

DOB does not currently allow the contractor to use a tower section until the CN is approved. DOB deems a tower section as a partial "tower crane erection". For this reason, the industry defaults to using templates. Previously, DOB authorized the contractors to use the first section as a template. It is the HRCO understanding that DOB is working to amend this restriction and allow a section to be used as outlined above.

The HRCO team witnessed instances where the installation team had to use shims and/or enlarge the bolt holes to attach the first section to the anchor stools. This practice places an additional bending moment on the bolted connection. The use of the first section will allow the installation team to plumb the tower prior to pouring the foundation, which will minimize the need to shim and enlarge bolt holes. Figure C.7.10 shows an anchor stool and tower section that illustrates the need to shim the tower to achieve plumbness.

The HRCO team observed one contractor that used half of a tower section as a template and one that made one from a non-rigid material (½" plywood) (site C-89 – 10/17/08).



Shims to level tower crane section

Because of shifted anchor-stool, the bolt holes had to be elongated so much, that an ordinary nut/washer could not be used any more. A steel plate was used instead.

Ordinary bolted connection, nut and washer used

**Figure C.7.10: Site C-55 – 10/9/08, examples of excessive shimming and bolt-hole elongation probably shifted.** 

#### **The crane user should install Original Equipment Manufacturer anchor stools whenever available**.

The practices in NYC are that the crane owner or user installs an anchor stool of their choice, and the licensed crane engineer designs anchor stools for particular cranes.

One custom (non-OEM) anchor stool was under-designed by the Crane Engineer of Record and required reinforcement prior to the crane being assembled.



**(Figure C.7.11: Site C-89 – 10/28/08, under designed anchor stool)** 

# **C.7.3.3 Additional Considerations for Good Practice**

The practice of designing a foundation prior to selection of a specific crane make, model and configuration leads to situations where special adapters must be designed to mate incompatible anchors and tower legs. It also creates the possibility for foundation design error (i.e., inaccurate and/or insufficient loads). The industry should move to a system in which the foundation is designed specifically for the crane that is actually used.

# **C.7.3.4 Additional HRCO Data**

Several jurisdictions and national standards have regulations that specifically address verification of the appropriate loads for foundations. For example:

**ASME B30.3-2004 Construction Tower Cranes** recommends that the first tower mast section be used and be secured before the concrete foundation is poured. If this cannot be done, the standard requires a template to be rigid and built so that the tower leg bearing surfaces are in the same plane.

**C-DAC - OSHA** The proposed OSHA rules in C-DAC, include the following:

### **\$1926.1435 Tower Cranes**

# *"(b) Erecting Climbing and Dismantling*

*(3) Foundations and structural supports. Tower crane foundations and structural supports shall be designed by the manufacturer or a registered professional engineer.* 

*(4) Addressing specific hazards ... In addition, the Assembly/Disassembly (A/D) supervisor shall address the following: (i) Foundations and structural supports. The A/D supervisor shall verify that tower crane foundations and structural supports are installed in accordance with their design."* 

**Singapore** requires new foundation anchors each time a tower crane is assembled. Further, the Ministry of Manpower circular OSHD / LE 1/08 implies that the foundation is inspection prior to the pouring of concrete;

**Britain** Uses an approach, where the HSE (Health and Safety Executive) similar to the American OSHA decided, that tower cranes have to be erected by the crane owner, who hands the erected crane over to the crane hirer. The crane hirer normally provides the tower crane foundation. Internal documents are used to assure the quality of the foundation. The HSE approved publication "Safe Use of Top Slew Tower Cranes" describes the procedure and shows an example:

"*This loading information should be used by the foundation designer employed by the user, to produce an adequate design, taking into account the ground conditions on site. Wherever a concrete pad, steel grillage, piled foundation or rail track is constructed to accept the loads from a TSTC, the contractor constructing the foundation should complete a foundation completion form to certify that the foundation has been correctly designed and constructed before erection of the crane starts."* 



 **Figure C.7.12: UK Certificate** 

The British Health and Safety Executive (HSE) approved publication "Maintenance Inspection and Thorough Examination of Tower Cranes; a Best Practice Guide" gives further information regarding the foundation inspection in section A11.12 (Foundation As–Built Report).

This report confirms that the foundations have been constructed in accordance with the foundation design (see summary in Table C.7.3). The report should be prepared by the organization that has constructed / installed the foundation. The appointed person responsible for the planning and supervision of the crane erection should countersign the report.



**Table C.7.3: Summary of the UK Foundation As-Built Report.**

**New Zealand** states the following requirements in the "Approved code of practice for cranes" published by the Department of Labour:

#### *"10.2 (6) Part 2: The inspection and testing of the tower crane after erection and annual inspection for recertification.*

*Inspections and testing will cover (but are not limited to) the following items. The following documentation is to be provided by the controller to the equipment inspector prior to testing commencing:* 

*(b) Foundation certificate, covering design and construction, from a chartered professional engineer and crack testing results of base anchors. IANZ-endorsed NDT reports are required."* 

# **C.7.4 Recommendation C-15: Load Test**

*The test weights to be used should not exceed the manufacturer's specification or, in case where the manufacturer is not available, the applicable ANSI standard should be followed..* 

# **C.7.4.1 Description**

A load test is part of DOB crane inspections (required by RS 19-2) for tower cranes. The test verifies that the crane, generally, is able to lift and hold the maximum rated load at the corresponding radii. Further, the installed safety devices warn the crane operator about a maximum load situation and eventually stop the lifting, booming, lowering and/or trolley out motions. The Engineer of Record for the Certificate of onsite inspection (CN) provides the load test procedure with eachapplication.



**Figure C.7.13: Load Test in Operation** 

In two cases a test load of the exact weight was not available on site, and the engineer of record provided a test procedure where the crane would have attempted to lift a test load exceeding the maximum allowable weight. In case of a malfunction of the safety devices that are to be tested, the crane could have been overloaded. In extreme cases this could cause catastrophic crane failure. In other cases, structural components and parts of the hoisting apparatus of the crane could have been overstressed, causing deformation, cracking or general weakening of crane components. These defects are often hidden and could heighten the risk of a catastrophic failure at a later date. In 2008, there was an incident that a crane dropped a load during a load test.

### **C.7.4.2 Recommendation Approach**

The Engineer of Record should include manufacturer recommendations or ANSI information when providing the load test procedure in the Certificate of on-site inspection (CN). In addition, the procedure should include:

- Line pull test should be performed on all gears
- A moment test should be performed as a standard practice for all load tests.
- All limit and pre-limit switches should be tested during the load test.

Inspectors from DOB witness all tower crane load tests. However, DOB has allowed procedures that could have overloaded the crane based upon the EOR's procedures included in the CN.

The HRCO moderated a conference of major crane manufacturers in November 2008. The manufacturers unanimously confirmed that load tests should be conducted with a test weight limited to the proper test load and that the crane should not be placed in a situation whereby it may become over-loaded. Similarly, ANSI standards B30.3 and B30.5 regarding load test states that the weight should not exceed 110% of the rated load.

Load test procedures submitted by engineers of record on C/N applications have created situations where the crane could have been overloaded as shown in Table 7-4. Further, load test procedures submitted by engineers of record for C/N application and reviewed by the HRCO team were contrary to the manufacturer's recommendation and the ANSI B30.3 standards by designing a protocol that the crane could have attempted to lift a weight 130% over the rate load should the safety features fail.

In three instances, the EOR did not include a moment over-load test. Cranes typically have two controlling load cases, maximum load and maximum moment. Both controlling cases must be checked to confirm the safety of the crane. Checking just one does not confirm whether the crane can safely operate under the other condition.

Reference Standards 19-2 (Paragraph 13.1) (dated September 14, 2006) requires that load ratings for climber tower cranes be conducted so that no structural member is overstressed.



**Table E.7.4: Review of Submitted Load Test Procedures**

# **C.7.4.3 Additional HRCO Observations**

The primary focus on the benchmarking activity on this recommendation was on standards published in the United States. Two such standards were developed by the American Society of Mechanical Engineers (B30.3 and B30.5). The tower crane standard (B30.3) primarily recommends that after erection (and climbing operations) all functional motion, limiting devices and brakes be tested prior to the operation. The static test load should be in the range of 102.5% to 110%, as recommended by the manufacturer. The Mobile crane standard (B30.5) requires a load test prior to the initial use or if load sustaining parts have been altered, replaced or repaired. The load test weight shall not exceed 110% of manufacturer's load rating.

In addition, manufacturers do not allow over loading the crane. Below is a portion of a load test procedure outlined in an OEM's operating manual.

*"Set the switch OS 11 "Hoist up": Attach the test load (minimum: permissible load at the end of the jib; maximum: permissible load at the end of the jib +10%).* 

*Set the switch OS 12 "Trolley forward": Attach the test load (minimum: maximum permissible load; maximum: maximum permissible load +10%)."* 

# **C.7.5 Recommendation C-5: Counterweights**

*Counterweight information should be readily available on the drawing and on the counterweight module itself.* 

### **C.7.5.1 Description**

Most tower cranes and larger mobile cranes rely on counterweights to provide stability. The complete counterweight is typically assembled from several counter weight modules. An error in the counterweight configuration or a malfunction of the mechanism that actuates movable counterweights can have catastrophic results. In addition, damaged concrete weights can present debris fall hazards.



 **Figure C. 7.14: Crane counter weights** 

# **C.7.5.2 Recommendation Approach**

Implementation of this recommendation should include the following actions:

- Require a clear description of the value and configuration of counterweight on the overview-drawing of the Certification of on-site Inspection (CN) submittal*.*
- Require each counterweight module to be labeled in a way that clearly and conveniently identifies the weight, including the assembled state (e.g. labels or stenciled number on the sides).
- Pay special attention to signs of corrosion and poor maintenance on the movable counterweight mechanisms.
- Enclose concrete counterweights to protect against damage and spalling.

#### **Require a clear description of the value and configuration of counterweight on the overview drawing of the Certification of on-site Inspection (CN) submittal.**

DOB does not require the Engineer of Record to include the counterweight configuration in the CN. However, details of other components are required such as height of tower and length of boom.

The HRCO observations shown in Table 7-5 identify that none of the reviewed CN's contained counterweight information. This is not unexpected since this is not a requirement. However, every project must have the CN plans on site and as such this would be the appropriate place for DOB, or special inspector, to review the information. Also, Figure C. 7.14 shows the location of various counter weights for two different cranes. The one on the left has markings and the one on the right has only one module labeled.

### **Require each counterweight module to be labeled in a way that clearly and conveniently identifies the weight, including the assembled state (e.g. labels or stenciled number on the sides).**

Current regulations do not require the counterweight value of each module be in a visible location. Further, DOB inspectors typically do not have the information to audit the installed counterweight configuration. Based on HRCO observations, the industry does not generally mark all counter weights in such a fashion that an Inspector can verify the designed configuration (weight and location). One out of the fifteen counterweight configuration has all modules marked in a visible manner (Figure C.7.14).

Table 7-5 provides data that indicate that the industry has not marked the counterweights in such a fashion that an Inspector can verify correct configurations (weight and location).

<b>Observation Type</b>	Number of <b>Observations</b>	<b>Observations</b> with Issue
CN's reviewed that did not have counter weight configurations	20	20
Counter weights without markings visible on all weights	15	14
Movable counter weight mechanism requiring maintenance	34	5

 **Table C.7.5: Counter Weight Issues** 

#### **Pay special attention to signs of corrosion and poor maintenance on the movable counterweight mechanisms***.*

Of the 34 tower cranes visited, five showed signs that the movable counter weight mechanism required some type of maintenance (i.e., excessive rust, rope required lubrication, etc.)



**Figure C.7.15: Serrated Counter Weight Sheaves (Site C-22, 9/4/08)** 



**Figure C.7.16: Rusted Counter Weight Sheave Posts (Site C-61, 11/5/08)** 

Cranes and Hoists C-64



**Figure C.7.17: Counter Weight Sheaves (Sites C-73 and C-76)** 

#### **Enclose concrete counterweights to protect against damage and spalling.**

The use on non-framed hanging concrete counter weights is limited in New York City. Hanging concrete counterweights deteriorate over time, and become cracked and/or damaged during handling, which could result in failure or spalling (see Figure C.7.18 from site C-6 – 7/3/08).



The counter weights shown are framed in steel. However, the frame on one shows severe rust

**Figure C.7.18: Encased Concrete Counterweights** 

### **C.7.5.3 Additional HRCO Data**

ASME and C-DAC contain provisions directly related to the counterweight recommendation:

#### **ASME B30.3 – 2004**

Construction Tower Cranes provides that the counter weight arrangement be pursuant to the manufacturer's specification and be guarded against shifting. The counter weight movement ropes should be inspected monthly, if one is provided.

#### **C-DAC**

The proposed new C-DAC rules include:

#### **§1926. 1435 Tower Cranes**

#### *"(b) Erecting Climbing and Dismantling*

#### *(8) Counterweight / Ballast*

*(i) Equipment shall not be erected, dismantled or operated without the amount and position of counterweight and/or ballast in place as specified by the manufacturer or a professional engineer familiar with the equipment.* 

*(ii) The maximum counterweight or ballast approved by the manufacturer or professional engineer familiar with the equipment shall not be exceeded."* 

The Committee also considered whether an operational aid in the form of counter weight sensors should be required on all equipment manufactured after January 1, 2008. Several Committee members representing crane manufacturers expressed concern as to the difficulty in developing a reliable counterweight sensor presently or in the near future. In light of these technological problems, the Committee did not include these.

# **C.7.6 Crane Design for Wind Effects**

This is not a formal recommendation, in that there is no indication that the current wind design basis of cranes in NYC is deficient. However, various countries are researching and considering revising their wind calculation requirements for temporary structures. This includes how wind affects tower and large mobile cranes. There are differences between US and European approaches to the development of wind forces on crane members. In addition, and as would be expected, the HRCO crane team observed that the older cranes were designed using an older wind standard (ANSI/ASCE 7-98), others by the newer standard (ANSI/ASCE 7-05), and some models used a combination of standards. A further study to determine the applicability of these standards should be considered.

A related HRCO recommendation for high-rise concrete construction indentifies the need for increased monitoring of actual wind speeds in Manhattan. Data from such monitoring should be used to assess the appropriateness of current crane design wind speeds.

# **C.7.7 Hoist Recommendation H-2: PE Sign-Off**

*Require the building engineer of record or an engineer acceptable to DOB to review that the building can support the loads imposed by the hoist.* 

# **C.7.7.1 Description**

There is no current requirement that a structural engineer review and sign-off on the applied building loads, nor is there a formal DOB engineering permitting review process. Consequently permits are approved by DOB and awarded to the contractor without engineering review of the hoist design, including the attachment to the building.

In most cases the Hoist Contractor does note directly on the drawings that the structure is "to be" or "must be" reviewed or evaluated by others. However, in most cases (73%) the HRCO hoist team has not been able to identify confirmation of any type of such review. Of the drawings that were available for review, most lacked sufficient information necessary for a proper review (particularly the loads imposed on the building structure by the hoist).

For those cases where a review was called for but not executed may be attributable to a number of causes. First, it informally appears that once the hoist drawings are prepared they are hastily submitted for permitting. Other cases may be attributed to the lack of judgment on the GC's part. Non-PE project managers may fail to properly value the importance of this review; because it can save money as well as potentially avoid a delay they decide to opt out of the review.

For the 27% of sites where the GC did provide proof of a review it was typically the result of due diligence by the General Contractor or their Project Manager. In these cases we've found that either the project manager was a Professional Engineer, the GC was unusually prudent or there was some discernible feature of the design warranting such a review. A discernible feature may be that the hoist or its supporting structure is bearing on a temporary structure or shoring, or some kind of cantilever part of the building. .

Three sites visited by the HRCO hoist team required additional shoring for supporting structure. This deficiency would likely have been identified during an engineering review.